



# Structured Uncertainty and Robust Performance

**ELEC 571L – Robust Multivariable Control**  
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**Honeywell**

# Outline

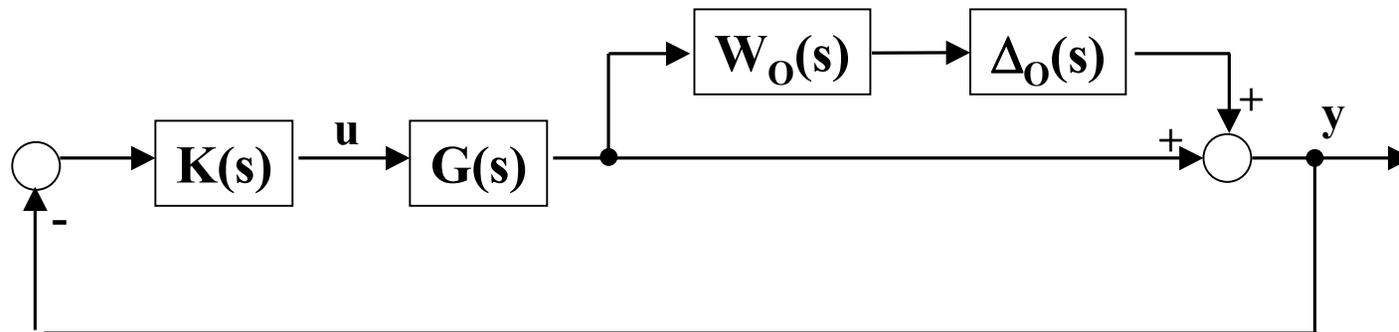
- **Structured uncertainty: motivating example.**
- **Structured singular value,  $\mu$ .**
- **Robust stability for structured uncertainty.**
- **Application of  $\mu$ : robust performance.**



# **Motivating Example**

## From last week...

- Consider the usual MIMO feedback loop with multiplicative output uncertainty:

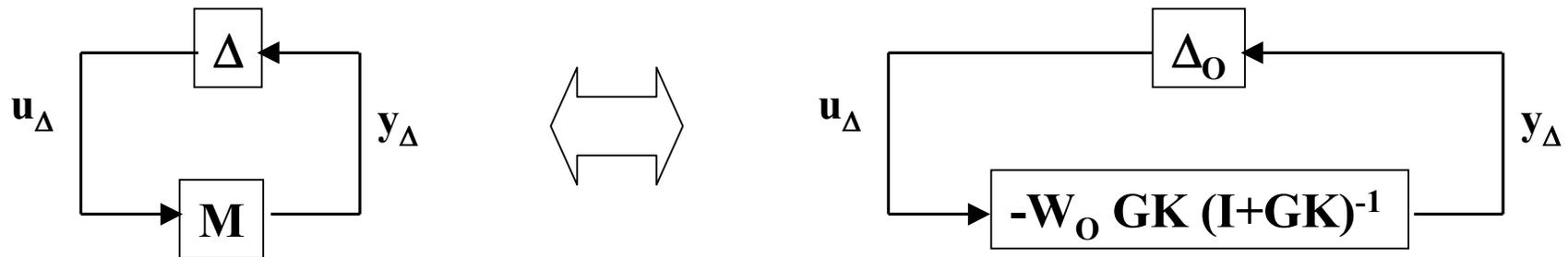


- the unstructured, stable transfer matrix  $\Delta_O(s)$  is bounded:

$$\|\Delta_O(s)\|_\infty \leq 1$$

# Robust Stability for Unstructured Uncertainty

- After massaging the block diagrams, we derived the  $M\Delta$  structure:

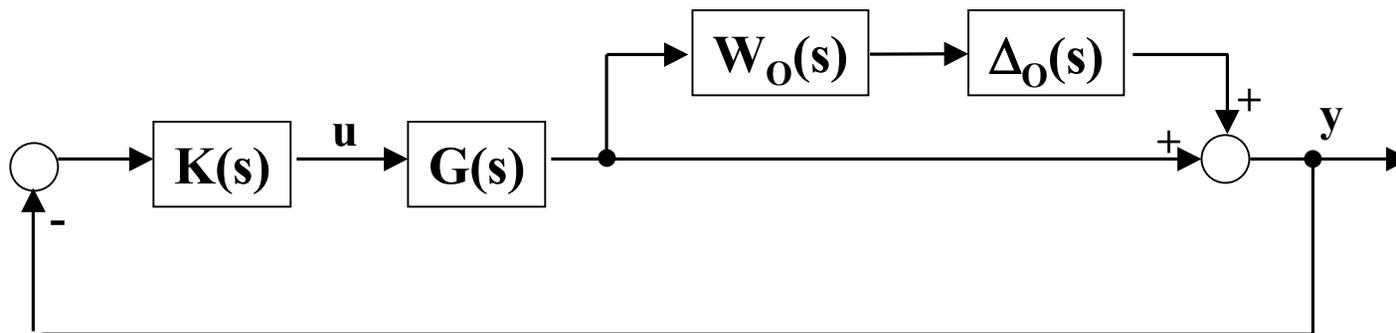


- and then said that “if we allow all  $\Delta_0$  such that  $\|\Delta_0\|_\infty \leq 1$ , then robust stability (RS) is given by NS and

$$\bar{\sigma}(W_0 \cdot GK[I + GK]^{-1}) < 1 \quad \text{for all } \omega$$

# Example

- **Assume:**
  - we have a 2-by-2 system (two actuators and two sensors).
  - we are very confident in our knowledge of our process.
  - However, the sensors were supplied by a very shady vendor (i.e. not Honeywell), and we only trust the readings by  $\pm 30\%$ .



## Example: model the uncertainty

- therefore we decide to go with:

$$W_o = \begin{bmatrix} 0.3 & 0 \\ 0 & 0.3 \end{bmatrix}, \quad \Delta_o = \begin{bmatrix} \Delta_1 & 0 \\ 0 & \Delta_2 \end{bmatrix}$$

where each diagonal element is **SISO** and bounded,

$$|\Delta_1(j\omega)| \leq 1, \quad |\Delta_2(j\omega)| \leq 1$$

giving the overall matrix  $\|\Delta_o\|_\infty \leq 1$ .

(see textbook Appendix for the proof!)

# Analysis

- Now suppose that at some frequency  $\omega$ , we find that  $M$  has the numerical values:

$$M = W_o \cdot GK[I + GK]^{-1}$$

$$= \begin{bmatrix} 0.1860 & 0.3719 \\ 0.5579 & 0.7438 \end{bmatrix}$$

# Analysis

- We then compute the maximum singular value and find

$$\begin{aligned}\bar{\sigma}(M(j\omega)) &= \bar{\sigma}\left(\begin{bmatrix} 0.1860 & 0.3719 \\ 0.5579 & 0.7438 \end{bmatrix}\right) \\ &= 1.0162\end{aligned}$$

- this is larger than 1 (and therefore violates last week's condition for RS).
- Does this mean we are not robustly stable?

# Analysis

- The answer is NO, we are not necessarily violating robust stability.
- What it DOES say, is that there exists SOME stable matrix  $\Delta_o(s)$  with  $\|\Delta_o\|_\infty \leq 1$ , such that the  $M\Delta$  structure is unstable.
- But this is NOT necessarily the same as failing RS!
- Maybe our uncertainty model does not permit the nasty, destabilizing perturbation  $\Delta_o(s)$ ?

# Uncertainty Structure

- Remember that, for this example, we are attempting to model sensor uncertainty only.
- We are considering only diagonal matrices  $\Delta_o(s)$ :

$$\Delta_o = \begin{bmatrix} \Delta_1 & 0 \\ 0 & \Delta_2 \end{bmatrix}$$

- The real question is: “Does there exist a diagonal matrix  $\Delta_o(s)$  that will destabilize the  $M\Delta$  structure?”

# Experimental Robust Stability

- We will do a numerical experiment.
- Given the nominal system,

$$M = \begin{bmatrix} 0.1860 & 0.3719 \\ 0.5579 & 0.7438 \end{bmatrix}$$

- Let us check the robust stability for
  - (1) full matrix perturbations,  $\Delta_{\text{full}}$
  - (2) diagonal matrix perturbations,  $\Delta_{\text{diag}}$

# Experimental Robust Stability

- Each of these perturbations satisfies the assumptions of Theorem 8.2.
- Which allows us to check RS by computing the maximum eigenvalue magnitude,

$$\rho(M\Delta) < 1$$

- In Matlab notation,

```
if max(abs(eig(M*Delta))) < 1
    'Delta is not destabilizing'
end
```

# Experimental Robust Stability

- 1. We create full complex matrix perturbations in Matlab with the commands:**

```
Delta_full = rand(n,n) + sqrt(-1)*rand(n,n);  
Delta_full = Delta_full /max(svd(Delta_full));
```

- 2. Diagonal matrix perturbations with the commands:**

```
Delta_diag = diag(rand(1,n)) + sqrt(-1)*diag(rand(1,n));  
Delta_diag = Delta_diag /max(svd(Delta_diag));
```

# Experimental Robust Stability

- Using the program “finddelta.m”, we tested robust stability using Theorem 8.2, for 1 000 000 randomly generated full and diagonal matrices.
- Results:

Perturbation	# Destabilizing	Percentage
$\Delta_{\text{full}}$	10 694	~1%
$\Delta_{\text{diag}}$	0	0%

# Experimental Robust Stability

- In a million examples, we found several full matrices  $\Delta_{\text{full}}$  which caused the system to be unstable.
- But we did not find a single destabilizing diagonal perturbation,  $\Delta_{\text{diag}}$  .
- This indicates (but does not prove) that we are safe from instability since we are only concerned with diagonal perturbations  $\Delta_{\text{diag}}$  .
- Look at Example 8.9 in your text for a related example.

# Experimental Robust Stability

In addition, these results also indicate (but do not prove) that the condition,

$$\bar{\sigma}(M) < 1$$

may be too conservative for use checking robust stability when we have knowledge of the structure of the perturbation  $\Delta$ .

# Structured Uncertainty

- In this case, we knew that  $\Delta$  was a diagonal matrix.
- This is common as robust control typically imposes a band-diagonal structure on the  $\Delta$ ,

$$\Delta = \begin{bmatrix} \Delta_1 & & & \\ & \Delta_2 & & \\ & & \ddots & \\ & & & \ddots \end{bmatrix}$$

with a separate  $\Delta_i$  for each independent source of uncertainty.



# **The Structured Singular Value**

# Structured Singular Value: Definition

Find the smallest allowable  $\Delta$  (measured in terms of  $\sigma(\Delta)$ ) which makes  $\det(I - M \Delta) = 0$ , then the **SSV** is defined as,

$$\mu(M(j\omega)) = \frac{1}{\bar{\sigma}(\Delta(j\omega))}$$

for  $\Delta \in \Pi$ , where  $\Pi$  is a set of structured perturbations (not necessarily  $\sigma(\Delta) \leq 1$ ).

# Robust Stability for Structured Uncertainty

Assume that the nominal system  $M$  and the perturbations  $\Delta$  are stable and  $\|\Delta\|_\infty \leq 1$ . Then the  $M\Delta$ -system is stable for all allowed perturbations if and only if,

$$\mu(M(j\omega)) < 1, \quad \text{for all } \omega$$

for all  $\Delta \in \Pi$ , where  $\Pi$  is the set of *allowable* perturbations.

## Example

- The m-file “calcmu.m” is a brute-force algorithm for computing  $\mu$ .
- We randomly generated 4 000 000 perturbing matrices  $\Delta_{\text{full}}$  and  $\Delta_{\text{diag}}$ .
- Then check to see the smallest matrices that destabilized the  $M\Delta$  system for our previous example.

## Example: full perturbations

- For  $\Delta_{\text{full}}$ , the smallest destabilizing perturbation (for frequency  $\omega$ ) was found at 0.9872, therefore:

$$\mu(M) \approx \frac{1}{0.9872} = 1.0130$$

- which indicates that (at this frequency) the system is not robustly stable for full perturbations with  $\|\Delta_{\text{full}}\|_{\infty} \leq 1$
- Remark: for full perturbations, we can verify this numerical value against the true  $\mu$ :  $\mu(M) = \bar{\sigma}(M) = 1.0162$ . So it is quite close!

## Example: structured perturbations

- For  $\Delta_{\text{diag}}$ , the smallest destabilizing perturbation was found at 1.0014, therefore:

$$\mu(M) \approx \frac{1}{1.0014} = 0.9986$$

- as expected, this number is smaller than for the full perturbations!
- and since it is smaller than 1, we then satisfy (at this frequency) robust stability for diagonal perturbations with  $\|\Delta_{\text{diag}}\|_{\infty} \leq 1$ .

## Structure: Special Cases

- In general,  $\mu(M) \leq \bar{\sigma}(M)$
- However, if the uncertainty set  $\Pi$  happens to contain the worst case perturbation  $\Delta$ , then we get equality

$$\mu(M) = \bar{\sigma}(M)$$

- The most common example of this is unstructured uncertainty,

$$\Pi = \{ \Delta: \|\Delta\|_{\infty} \leq 1 \}$$

## Structure: Special Cases

- **Multiple sources of uncertainty.** Typically resulting in a block-diagonal  $\Delta$ :

$$\Pi = \{ \Delta = \text{diag}\{\Delta_1, \Delta_2, \dots\} : \|\Delta_i\|_\infty \leq 1 \}$$

- **Parametric uncertainty.** Typically resulting in real  $\Delta$ :

$$\Pi = \{ \Delta \in \mathfrak{R} : -1 \leq \Delta \leq 1 \}$$

## Computation of $\mu(M)$

- Unfortunately it is not straightforward to compute  $\mu(M)$  in general.
- Various methods exist for computing  $\mu(M)$ .
- Methods often depend on the structure of  $\Delta$  and  $M$ .
- It is worth reading Sections 8.8.2 and 8.8.3 to see results for some special cases which arise in practical work.



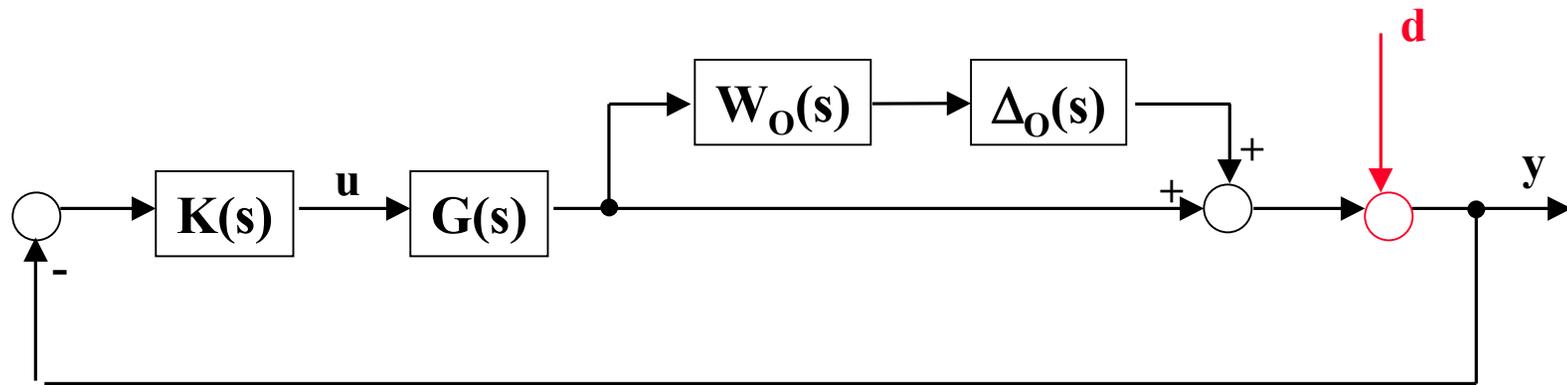
# **The Structured Singular Value and Robust Performance**

## Application: Robust Performance with $\mu$

- We just discussed using the  $\mu(M)$  to test for robust stability (RS).
- If we reconfigure our blocks, we can apply the same concepts to test for robust performance (RP).

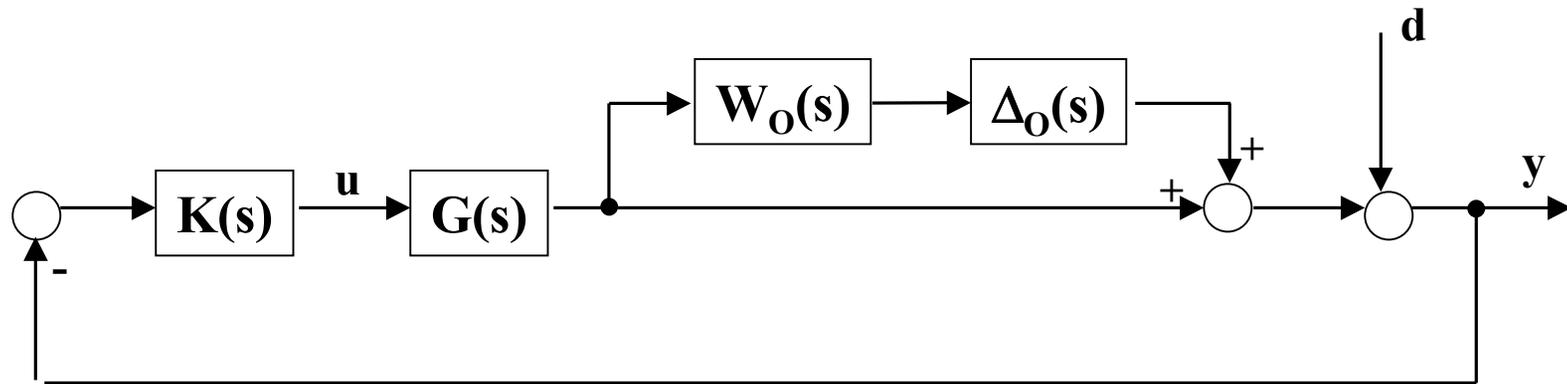
# Our usual system

- Take our usual system with multiplicative output uncertainty:



- The only new feature is the additive output disturbance,  $d$ .

# Define Performance



- We will use a familiar definition of performance:

$$\bar{\sigma}(W_p S) < 1$$

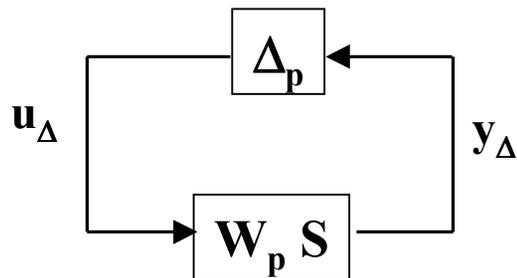
- where the sensitivity function  $S = [I + G_p K]^{-1}$ .
- $W_p$  is typically a low-pass filter (often an integrator).

# Re-interpret Performance

- Note that, the performance specification:

$$\bar{\sigma}(W_p S) < 1$$

- Can be re-written as a RS condition using a fictitious perturbation  $\Delta_p$ :

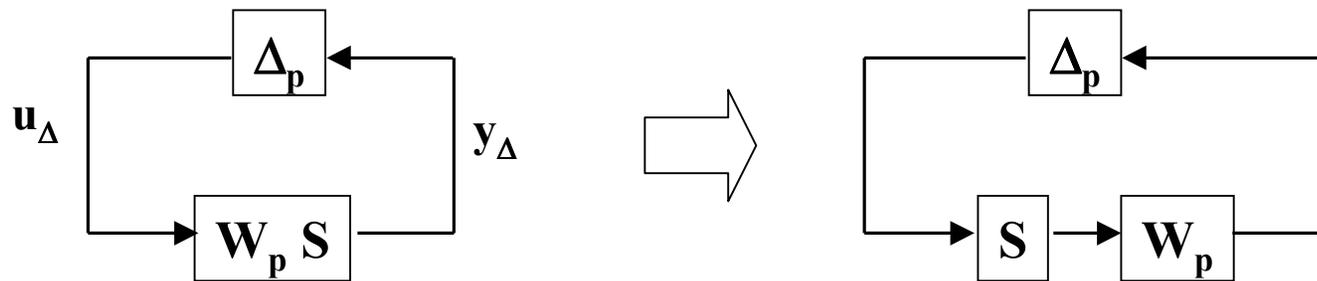


RS  
⇔

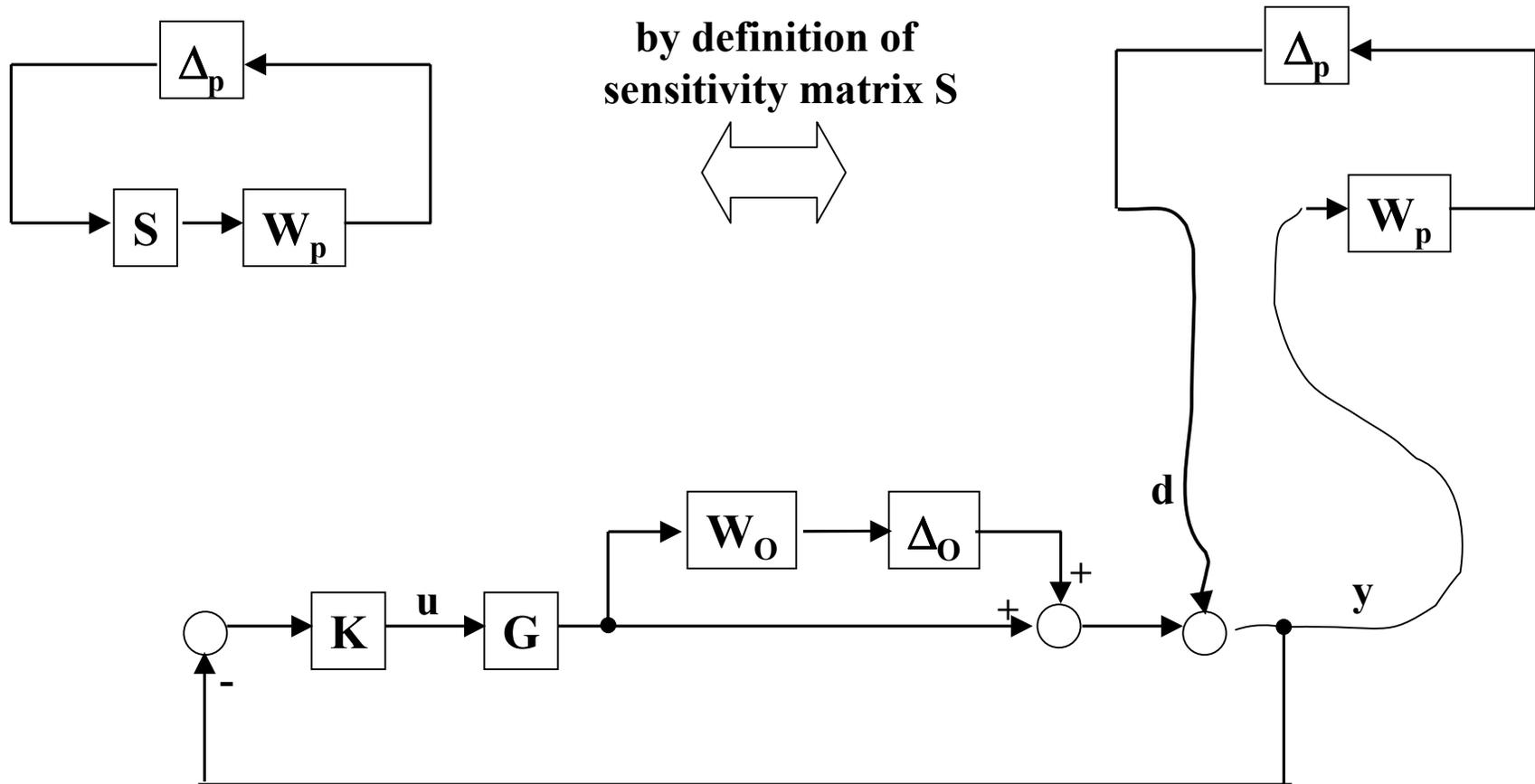
$$\bar{\sigma}(W_p S) < 1$$

with  $\|\Delta_p\|_\infty \leq 1$

# Reconfiguring

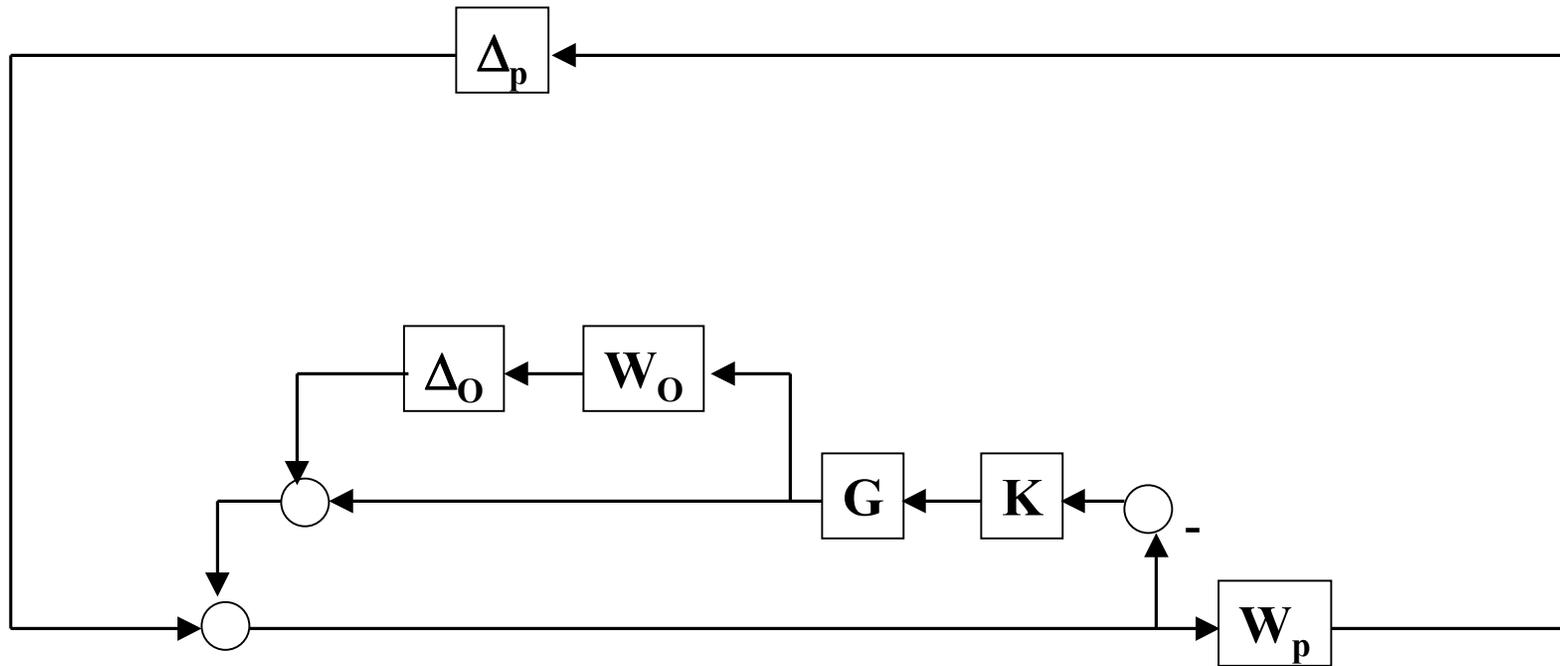


# Reconfiguring

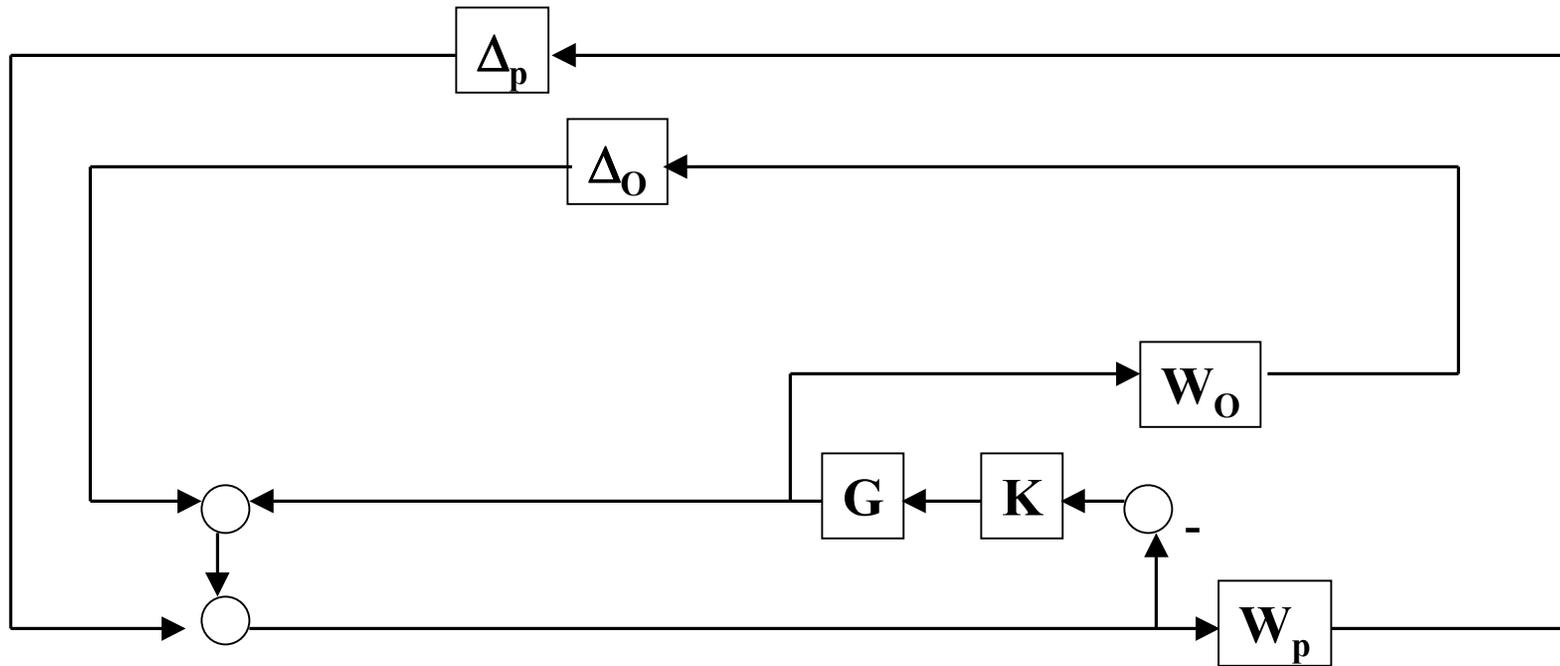


- which now has two deltas:
  - $\Delta_o$  for model uncertainty,
  - $\Delta_p$  for performance.

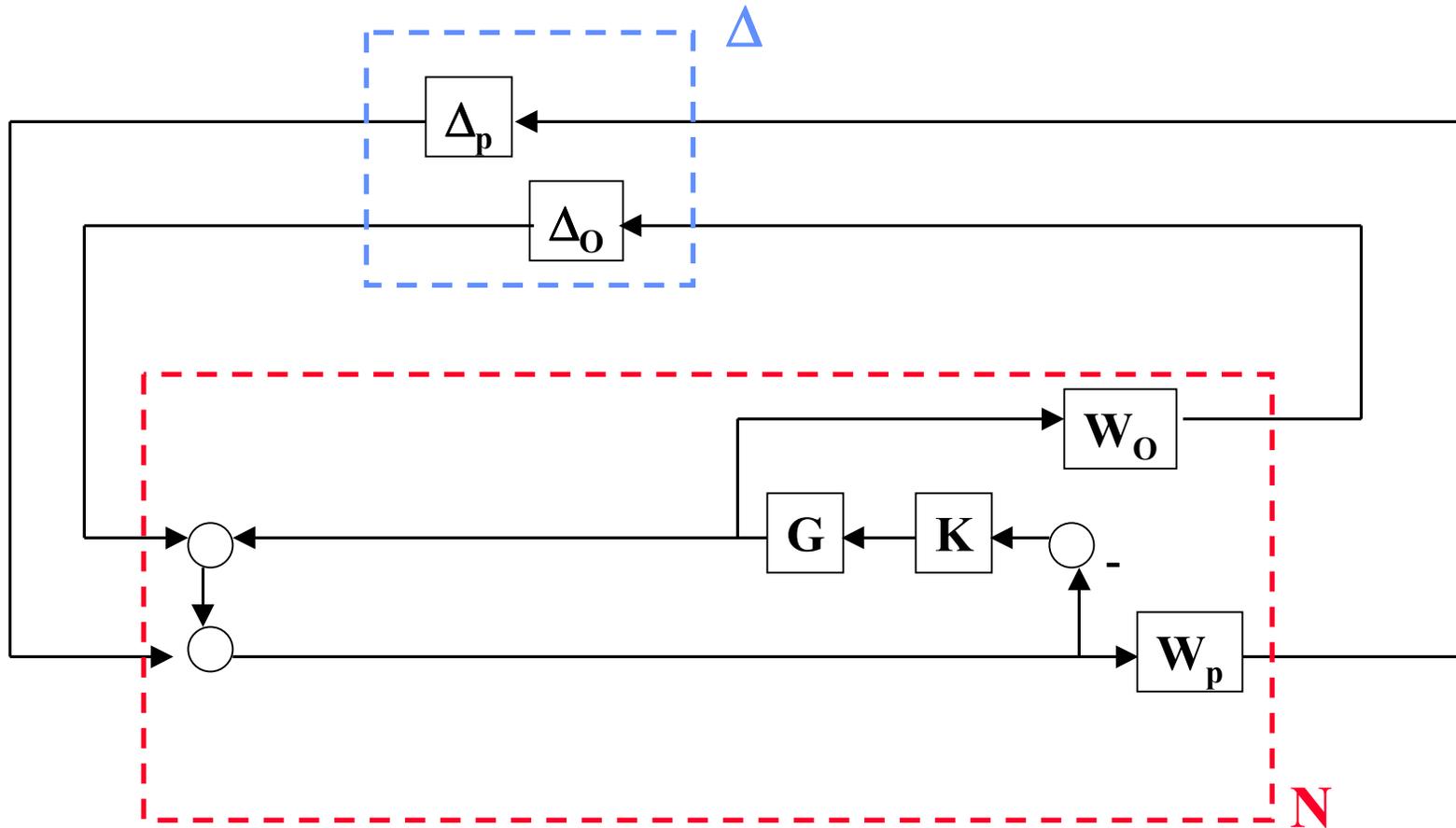
# Massaging Block Diagram



# Massaging Block Diagram



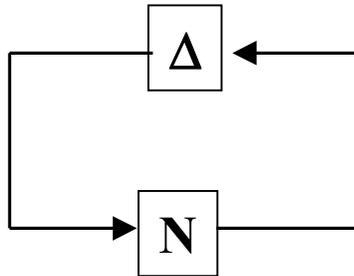
# Massaging Block Diagram



- this is known as  $N\Delta$ -structure, because of the  $N$  and the  $\Delta$ .

# Computing N and $\Delta$

- Using the same familiar techniques we can compute:



- with the factors:

$$\Delta = \begin{bmatrix} \Delta_o & \\ & \Delta_p \end{bmatrix}$$

$$N = \begin{bmatrix} -W_o GK[I + GK]^{-1} & -W_o GK[I + GK]^{-1} \\ W_p [I + GK]^{-1} & W_p [I + GK]^{-1} \end{bmatrix}$$

# Equivalence!

- **The performance condition:**

$$\bar{\sigma}(W_p S) < 1, \quad \text{for all } G_p$$

- **has been transformed into the structured singular value condition:**

$$\mu(N) < \frac{1}{\bar{\sigma}(\Delta)}$$

**with the “uncertainty” given by,**

$$\Delta = \begin{bmatrix} \Delta_o & \\ & \Delta_p \end{bmatrix} \quad \|\Delta_o\|_\infty \leq 1, \quad \|\Delta_p\|_\infty \leq 1$$

# Comments

- There may be several layers of uncertainty.
- For example, the uncertainty perturbation  $\Delta_O$  may have further structure:
  - $\Delta_O = \Delta_{\text{full}}$       full matrix (i.e. unstructured)
  - $\Delta_O = \Delta_{\text{diag}}$       diagonal matrix
- The  $\mu$ -condition can be applied to a wide variety of RP problem statements.
- See Section 8.10 for general procedure.

# Conclusions

- The structure of model uncertainty is defined during modelling.
- If a destabilizing perturbation is small but is not included in the allowable structure, then it is not considered a violation of robust stability.
- The structured singular value ( $\mu$ ), is a non-conservative definition of robust stability.
- Computing  $\mu$  typically requires approximation, and the computation may introduce conservativeness.

# Conclusions

- **The structured singular value  $\mu$  is a powerful tool for robust control.**
- **Results were derived for robust stability (RS) and robust performance (RP).**