

ELEC 343, Home Work Assignment # 1:

Follow through Example 1A, and do Study Problem, SP1.2-2, SP1.2-4

Follow through Example 1B, and do Study Problems SP1.3-1, SP1.3-3

Follow through Example 1D, and do Study Problems SP1.5-2 and SP1.5-3.

Textbook Chapter Problem(s): 3, 8, 9, 15, and 16.

Solutions:

SP1.2-2

From SP1.2-1, we have phasors of voltage and current:

$$\tilde{V} = 1 \angle 0^\circ, \quad \tilde{I} = 1 \angle 180^\circ$$

Then we have $\omega = 2\pi \cdot 60 \approx 377$ rad/s

$$v = \sqrt{2} \cdot \cos(\omega t) = \sqrt{2} \cdot \cos(377 \cdot t)$$

$$i = \sqrt{2} \cdot \cos(\omega t + \pi) = \sqrt{2} \cdot \cos(377 \cdot t + \pi)$$

$$p = v \cdot i = \sqrt{2} \cdot \cos(377 \cdot t) \cdot \sqrt{2} \cdot \cos(377 \cdot t + \pi)$$

$$= 2 \left(\frac{1}{2} \cos(754 \cdot t + \pi) + \frac{1}{2} \cos(-\pi) \right) =$$

$$= -1 + \cos(754 \cdot t + \pi)$$

SP 1.2-4 For simplicity, and without lack of generality, neglect resistance and assume the voltage is along the real axis. In this case the relationship between voltage and current is given by:

$$V \angle 0 = j(X_L - X_C) \tilde{I} + \tilde{E}$$

One can observe that the magnitude and phase of \tilde{E} controls the magnitude and direction of \tilde{I} . For example, if $\tilde{E} = 2 \angle 0^\circ$ and $X_L > X_C$, \tilde{I} will lead \tilde{V} . In contrast, if $\tilde{E} = 0.5 \angle 0^\circ$ and $X_L > X_C$, \tilde{I} will lag \tilde{V} .

SP1.3-1. $Ni = \mathcal{R}_{ab}(\Phi_1 + \Phi_2) + \mathcal{R}_{bcda} \Phi_1$

$$\Phi_1 = \frac{1}{\mathcal{R}_{bcda}} [Ni - \mathcal{R}_{ab}(\Phi_1 + \Phi_2)]$$

$$\Phi_1 = \frac{1}{358,099} \left[-(109,419)(2.547 \times 10^{-3}) \right] = 2.014 \times 10^{-3} \text{ Wb}$$

SP1.3-3. With windings as shown in Fig. 1B-1 and with the center leg removed, the total mmf is

$$\text{mmf}_t = \text{mmf}_1 + \text{mmf}_2 = N_1 I_1 + N_2 I_2$$

$$= (150)(9) + (90)(-15) = 0$$

SP1.5-2. During steady-state conditions, the time rate-of-change of i_1 is zero; therefore, a voltage is not induced in the 2-winding. Hence, for the 2-winding open or short

circuited $I_1 = \frac{V}{r_1} = \frac{12}{6} = 2 \text{ A}$ and $I_2 = 0$.

SP1.5-3. $Z = r_1 + j\omega_e(L_{l1} + L_{m1}) = 6 + j(100)(13.5 + 263.9) \times 10^{-3}$

$$= 6 + j27.74 = 28.38 \angle 77.8^\circ$$

$$\tilde{I}_1 = \frac{\tilde{V}_1}{Z} = \frac{10 \angle 0^\circ}{28.38 \angle 77.8^\circ} = 0.352 \angle -77.8^\circ \text{ A}$$

3. The reluctance of the iron is

$$\mathcal{R}_m = \frac{l}{\mu_0 \mu_r A} = \frac{(4)(0.25)}{(4000)(4\pi \times 10^{-7})(0.05)^2} = 79,577 \text{ H}^{-1}$$

$$L_{12} = \frac{N_1 N_2}{\mathcal{R}_m} = \frac{(50)(100)}{79,577} = 0.0628 \text{ H}$$

$$L_{m1} = \frac{N_1^2}{\mathcal{R}_m} = \frac{50^2}{79,577} = 0.0314 \text{ H}$$

$$L_{m2} = \frac{N_2^2}{\mathcal{R}_m} = \frac{100^2}{79,577} = 0.1257 \text{ H}$$

8. $\tilde{V}_1 = \frac{10}{2\sqrt{2}} \angle 0^\circ = 3.54 \angle 0^\circ \text{ V}$

$$Z = r_1 + r_2 + j\omega_e(L_{l1} + L_{l2}) = 10 + 10 + j(2\pi)(30)(30 + 30) \times 10^{-3}$$

$$= 20 + j11.31 \Omega$$

$$\tilde{I}_1 = \frac{\tilde{V}_1}{Z} = \frac{3.54 \angle 0^\circ}{20 + j11.31} = 0.154 \angle -29.5^\circ \text{ A}$$

9. Since $\omega_e = 400$, $X_{m1} = 400 \Omega$. Neglecting the magnetizing current $i_1 = -i_2$.

(a) $\tilde{V}_1 = \frac{2}{\sqrt{2}} \angle 0^\circ = \sqrt{2} \angle 0^\circ$

$$\tilde{I}_1 = \frac{\tilde{V}_1}{(r_1 + r_2 + R_L) + j\omega_e(L_{l1} + L_{l2})} = \frac{\sqrt{2} \angle 0^\circ}{4 + j(400)(0.02)} = 0.158 \angle -63.4^\circ \text{ A}$$

(b) $I_1 = \sqrt{2} 0.158 \cos(400t - 63.4^\circ)$

$$15. L_m(x) = \frac{k}{k_0 + x}$$

$$k = \frac{N^2 \mu_0 A_i}{2} = \frac{(500)^2 (4\pi \times 10^{-7})(4 \times 10^{-4})}{2} = 2\pi \times 10^{-5}$$

$$k_0 = \frac{l_i}{2\mu_{Ti}} = \frac{20 \times 10^{-2}}{(2)(1000)} = 10^{-4}$$

$$L_m(x) = \frac{2\pi \times 10^{-5}}{10^{-4} + x} H$$

The approximation for $x > 0$ is

$$L_m(x) = \frac{2\pi \times 10^{-5}}{x} H$$

Now to find minimum value of x

$$\frac{2\pi \times 10^{-5}}{x} = 1.1 \frac{2\pi \times 10^{-5}}{10^{-4} + x}$$

Solving for x yields $x = 1$ mm. Thus, the approximate expression is 10% in error at $x = 1$ mm and less than this for $x > 1$ mm.

$$16. L_m(x) = \frac{k}{k_0 + x}$$

$$\frac{\partial L_m(x)}{\partial x} = \frac{-k}{(k_0 + x)^2}$$

$$v = r i + (L_1 + \frac{k}{k_0 + x}) \frac{di}{dt} - i \frac{k}{(k_0 + x)^2} \frac{dx}{dt}$$

$$v = r \sqrt{2} I_s \cos \omega_e t - (L_1 + \frac{k}{k_0 + t}) \omega_e \sqrt{2} I_s \sin \omega_e t - \sqrt{2} I_s \cos \omega_e t \left[\frac{k}{(k_0 + t)^2} \right]$$

Gathering terms

$$v = \left[r - \frac{k}{(k_0 + t)^2} \right] \sqrt{2} I_s \cos \omega_e t - (L_1 + \frac{k}{k_0 + t}) \omega_e \sqrt{2} I_s \sin \omega_e t$$

Taking the limit as $t \rightarrow \infty$

$$v = r \sqrt{2} I_s \cos \omega_e t - L_1 \omega_e \sqrt{2} I_s \sin \omega_e t$$

which is the voltage equation for a linear r-L circuit. In phasor form,

$$\tilde{V} = (r + j \omega_e L_1) \tilde{I}$$