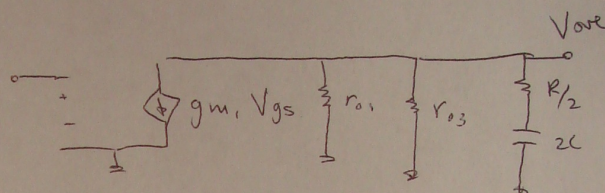
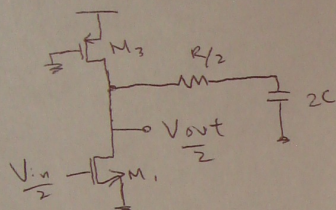


Year 2011 ECE 488 Assignment 3 Solution.

Q1.

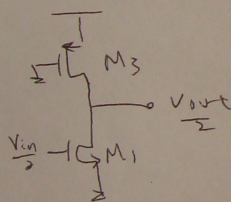
i). Half circuit:



$$A_v = -g_{m1} (r_{o1} \parallel r_{o3} \parallel (\frac{R}{2} + \frac{1}{s2C}))$$

ii) Very low frequency means capacitor acts as open circuit.

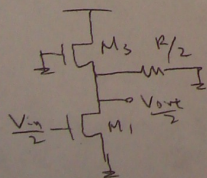
Half circuit:



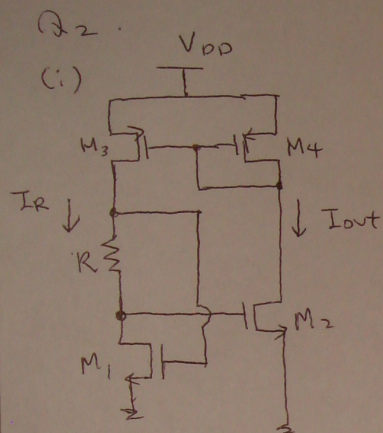
$$A_v = -g_{m1} (r_{o1} \parallel r_{o3})$$

iii) Very high frequency means capacitor acts as short circuit.

Half circuit



$$A_v = -g_{m1} (r_{o1} \parallel r_{o3} \parallel \frac{R}{2})$$



$$\left(\frac{W}{L}\right)_3 = \left(\frac{W}{L}\right)_4 \quad \lambda = \gamma = 0.$$

All transistors in saturation..

$$I_{D3} = \frac{1}{2} \mu_p C_{ox} \left(\frac{W}{L}\right)_3 (|V_{gs3}| - |V_{thp}|)^2$$

$$I_{D4} = \frac{1}{2} \mu_p C_{ox} \left(\frac{W}{L}\right)_4 (|V_{gs4}| - |V_{thp}|)^2$$

$$|V_{gs3}| = |V_{gs4}|$$

$$\Rightarrow I_{D3} = I_{D4}$$

$$\therefore I_R = I_{out} \quad \therefore I_{D1} = I_{D2}$$

$$I_R = \frac{V_{gs1} - V_{gs2}}{R}$$

$$I_{D1} = I_{D2} = I_{out} = \frac{1}{2} \mu_n C_{ox} \left(\frac{W}{L}\right)_2 (V_{gs2} - V_t)^2$$

$$\Rightarrow V_{gs2} = \sqrt{\frac{2 I_{out}}{\mu_n C_{ox} \left(\frac{W}{L}\right)_2}} + V_t$$

$$V_{gs1} = \sqrt{\frac{2 I_{out}}{\mu_n C_{ox} \left(\frac{W}{L}\right)_1}} + V_t$$

substitute

$$\Rightarrow R \cdot I_{out} = \sqrt{\frac{2 I_{out}}{\mu_n C_{ox} \left(\frac{W}{L}\right)_1}} - \sqrt{\frac{2 I_{out}}{\mu_n C_{ox} \left(\frac{W}{L}\right)_2}}$$

Assume

$$\left(\frac{W}{L}\right)_2 = K \left(\frac{W}{L}\right)_1$$

where K is a constant.

(ii) No change because I_{out} doesn't depend on V_{DD} .

$$= \sqrt{\frac{2 I_{out}}{\mu_n C_{ox} \left(\frac{W}{L}\right)_1}} \left(1 - \frac{1}{\sqrt{K}}\right)$$

$$I_{out} = \frac{2}{\mu_n C_{ox} \left(\frac{W}{L}\right)_1} \cdot \frac{1}{R^2} \cdot \left(1 - \frac{1}{\sqrt{K}}\right)^2$$

(iii) No change since no body effect, because bulks are connected to S.

Q3. Total power consumed $P = 3 \text{ mW} = I \cdot V_{DD}$. $V_{DD} = 3 \text{ V}$
 $V_t = 0.5 \text{ V}$
 $\Rightarrow I_{\text{total}} = \frac{3 \text{ mW}}{3 \text{ V}} = 1 \text{ mA}$.

It's given that bias current for stage 1 and 2 are equal,

so $I_{D0} = 0.5 \text{ mA}$ and $I_{D6} = 0.5 \text{ mA} = I_{D5}$

Swing = 2.6 V , and allocate equal overdrive voltage to M_5 &

M_6 , means $V_{ov5} = V_{ov6} = 0.2 \text{ V}$. $\Rightarrow V_{\text{bias1}} - V_t = 0.2 \text{ V}$
 $\Rightarrow V_{\text{bias1}} = 0.7 \text{ V}$.

$I_{D5} = 0.5 \text{ mA} = \frac{1}{2} \mu_p C_{ox} \frac{W_{p5}}{L} (V_{ov5})^2$ $\mu_p C_{ox} = 0.5 \text{ mA/V}^2$

$L = 0.4 \mu\text{m}$

$\Rightarrow W_{p5} = 20 \mu\text{m}$

$\mu_n C_{ox} = 1 \text{ mA/V}^2$

$I_{D6} = \frac{1}{2} \mu_n C_{ox} \frac{W_{n6}}{L} (V_{ov6})^2 \Rightarrow W_{n6} = \frac{2 I_{D6} \cdot L}{\mu_n C_{ox} (V_{ov6})^2} = 10 \mu\text{m}$

Assume all transistors in stage 1 (differential amplifier) are perfectly matched, $\Rightarrow I_{D3} = I_{D4} = 0.25 \text{ mA} = I_{D1} = I_{D2}$

$W_{p3} = \frac{2 I_{D3} \cdot L}{\mu_p C_{ox} (V_{ov3})^2}$

$= 10 \mu\text{m} = W_{p4}$

since $V_{sg3} = V_{sg5} \Rightarrow V_{ov3} = V_{ov5} = 0.2 \text{ V}$
 $\uparrow$ given.

Total gain $A_v = 1000$

$A_v \approx g_{m2} (r_{o2} \parallel r_{o4}) \cdot g_{m5} (r_{o5} \parallel r_{o6})$

$r_o = \frac{1}{\lambda I_o} \Rightarrow r_{o2} = 40 \text{ k}\Omega$

$r_{o4} = 40 \text{ k}\Omega$ $r_{o5} = 20 \text{ k}\Omega$

$r_{o6} = 20 \text{ k}\Omega$

$g_{m5} = \mu_p C_{ox} \frac{W_{p5}}{L} (V_{ov5}) = 5 \text{ mS}$

plug in A_v equation $\Rightarrow g_{m2} = 1 \text{ mS}$

$g_{m2} = \frac{2 I_{D2}}{V_{gs2} - V_t} = \frac{2 I_{D2}}{V_{gs2} - V_t} = \frac{2 I_{D2}}{V_{ov2}} = \frac{g_{m2}}{0.5 \text{ V}}$

$W_{n0} = \frac{2 I_{D0} \cdot L}{\mu_n C_{ox} (V_{ov0})^2}$
 $= 10 \mu\text{m}$
 $\uparrow$
 $V_{ov0} = V_{ov6}$
 because same V_{gs} .

$\downarrow$
 $W_{n2} = W_{n1} = \frac{2 I_{D2} \cdot L}{\mu_n C_{ox} (V_{gs2} - V_t)^2}$
 $= 0.8 \mu\text{m}$.