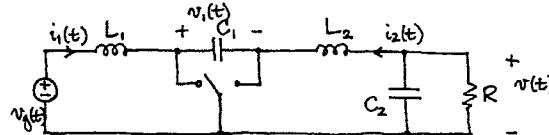


Problem 7.6

Ideal Cuk converter in CCM:



(a) Averaged nonlinear equations:

$$L_1 \frac{d\langle i_1 \rangle_{T_S}}{dt} = \langle v_g \rangle_{T_S} - d' \langle v_i \rangle_{T_S}$$

$$C_1 \frac{d\langle v_i \rangle_{T_S}}{dt} = d' \langle i_1 \rangle_{T_S} - d \langle i_2 \rangle_{T_S}$$

$$L_2 \frac{d\langle i_2 \rangle_{T_S}}{dt} = \langle v \rangle_{T_S} + d \langle v_i \rangle_{T_S}$$

$$C_2 \frac{d\langle v \rangle_{T_S}}{dt} = - \langle i_2 \rangle_{T_S} - \frac{\langle v \rangle_{T_S}}{R}$$

Small signal AC equations:

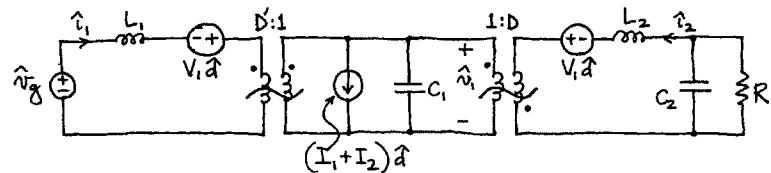
$$L_1 \frac{d\hat{i}_1}{dt} = \hat{v}_g - D \hat{i}_1 + V_i \hat{a}$$

$$C_1 \frac{d\hat{v}_i}{dt} = D \hat{i}_1 - D \hat{i}_2 - (I_1 + I_2) \hat{a}$$

$$L_2 \frac{d\hat{i}_2}{dt} = \hat{v} + D \hat{i}_1 + V_i \hat{a}$$

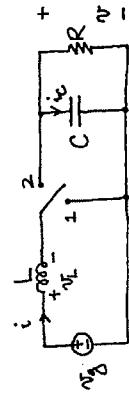
$$C_2 \frac{d\hat{v}}{dt} = - \hat{i}_2 - \frac{\hat{v}}{R}$$

(b) Small signal AC equivalent circuit

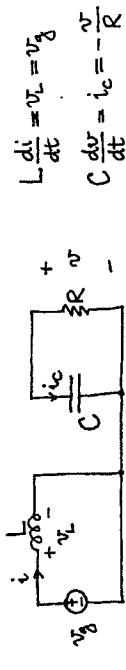


Problem 7.1

Ideal boost converter in CCM:



(a) Switch in position 1 ,  $0 < t \leq dT_s$

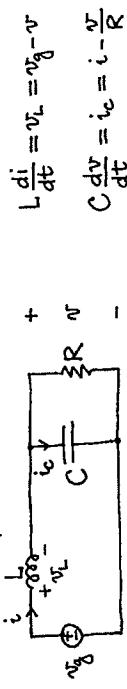


Small-ripple approximation:

$$L \frac{d\langle i(t) \rangle_{T_s}}{dt} = \langle v_g(t) \rangle_{T_s}$$

$$C \frac{d\langle v_r(t) \rangle_{T_s}}{dt} = -\frac{\langle v_r(t) \rangle_{T_s}}{R}$$

Switch in position 2 ,  $dT_s < t \leq T_s$



Small ripple approximation:

$$L \frac{d\langle i(t) \rangle_{T_s}}{dt} = \langle v_g(t) \rangle_{T_s} - \langle v_r(t) \rangle_{T_s}$$

$$C \frac{d\langle v_r(t) \rangle_{T_s}}{dt} = \langle i(t) \rangle_{T_s} - \frac{\langle v_r(t) \rangle_{T_s}}{R}$$

Nonlinear averaged equations:

$$L \frac{d\langle i \rangle_{T_s}}{dt} = d\langle v_g \rangle_{T_s} + d'(\langle v_g \rangle_{T_s} - \langle v_r \rangle_{T_s})$$

$$= \langle v_g \rangle_{T_s} - d'\langle v_r \rangle_{T_s}$$

$$C \frac{d\langle v_r \rangle_{T_s}}{dt} = d\left(-\frac{\langle v_r \rangle_{T_s}}{R}\right) + d'\left(\langle i \rangle_{T_s} - \frac{\langle v_r \rangle_{T_s}}{R}\right)$$

$$= d' \langle i \rangle_{T_s} - \frac{\langle v_r \rangle_{T_s}}{R}$$

(b) Perturb and linearize. Let

$$\langle v_g \rangle_{T_s} = V_g + \hat{v}_g(t)$$

$$d(t) = D + \hat{d}(t)$$

$$\langle i \rangle_{T_s} = I + \hat{i}(t)$$

$$\langle v_r \rangle_{T_s} = V + \hat{v}(t)$$

then

$$L \frac{d}{dt} (I + \hat{i}(t)) = V_g + \hat{v}_g(t) - (D' - \hat{d}(t))(V + \hat{v}(t))$$

Large signal DC components:

$$O = V_g - DV$$

1st order AC terms:

$$L \frac{d\hat{i}}{dt} = \hat{v}_g(t) - D' \hat{v}(t) + V \hat{d}(t)$$

$$C \frac{d}{dt} (V + \hat{v}(t)) = (D' - \hat{d}(t))(I + \hat{i}(t)) - \frac{V + \hat{v}(t)}{R}$$

Large signal DC components

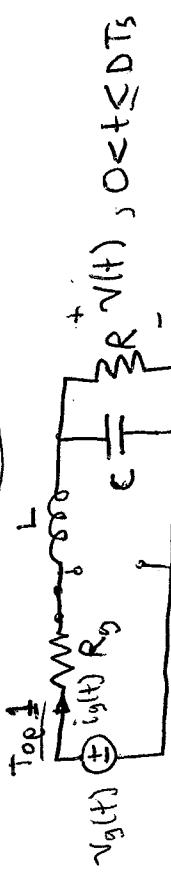
$$O = D' I - V/R$$

1st order AC terms:

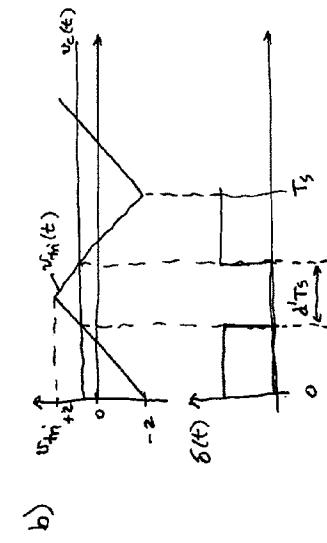
$$C \frac{d\hat{v}}{dt} = D' \hat{I}(t) - I \hat{d}(t) - \frac{\hat{V}(t)}{R}$$

**Problem 7.8**

a, b



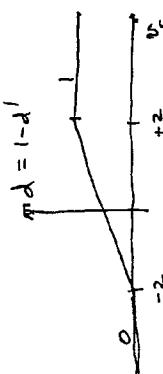
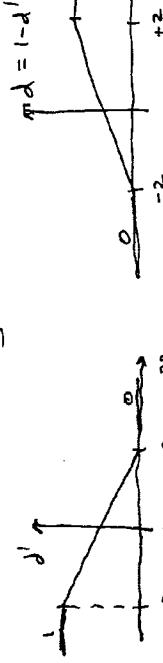
a)  $T_s = 50\mu s$  so  $f_s = \frac{1}{50\mu s} = 20 \text{ kHz}$



$d' = 0$  when  $v_c = +2$

$d' = 1$  when  $v_c = -2$

$d'$  varies linearly with  $v_c$



$$d = \begin{cases} 1 & \text{for } v_c \geq 2 \\ \frac{v_c + 1}{4} & \text{for } -2 \leq v_c \leq +2 \\ 0 & \text{for } v_c \leq -2 \end{cases}$$

The gain  $\frac{d}{v_c}$  is  $\frac{1}{4}$  is valid for  $-2 \leq v_c \leq +2$  (c)

Top 1

$$* \mathcal{N}_L(t) = L \cdot \frac{d i_L(t)}{dt} = V_g - L \cdot R_g - v(t) \quad * i_L(t) = C \frac{dv(t)}{dt} = i_L - \frac{v}{R}$$

\*  $i_g = i_L$

Top 2

$$* \mathcal{N}_L(t) = L \cdot \frac{d i_L(t)}{dt} = -v(t) \quad * i_L(t) = C \frac{dv(t)}{dt} = i_L - \frac{v}{R} \quad * i_g = 0$$

Top 1

$$\begin{bmatrix} L & 0 \\ 0 & C \end{bmatrix} \begin{bmatrix} i_L \\ v_c \end{bmatrix} = \underbrace{\begin{bmatrix} -R_g - 1 \\ 1 - 1/R \end{bmatrix}}_{A_1} \begin{bmatrix} i_L \\ v_c \end{bmatrix} + \underbrace{\begin{bmatrix} 1 \\ 0 \end{bmatrix}}_{B_1} [V_g]$$

Top 2

$$\begin{bmatrix} L & 0 \\ 0 & C \end{bmatrix} \begin{bmatrix} i_L \\ v_c \end{bmatrix} = \underbrace{\begin{bmatrix} 0 & -1 \\ 1 - 1/R & 0 \end{bmatrix}}_{A_2} \begin{bmatrix} i_L \\ v_c \end{bmatrix} + \underbrace{\begin{bmatrix} 0 \\ 0 \end{bmatrix}}_{B_2} [V_g]$$

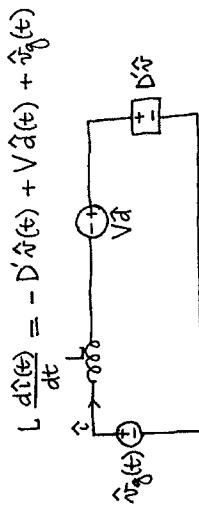
$$[i_g] = \underbrace{\begin{bmatrix} 1 & 0 \end{bmatrix}}_{C_1} \begin{bmatrix} i_L \\ v_c \end{bmatrix} + \underbrace{\begin{bmatrix} 0 \\ 0 \end{bmatrix}}_{E_1} [V_g]$$

7.8 (cont)

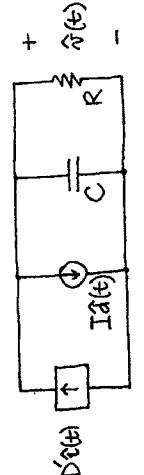
- \* Averaged matrices  
 $(D+D') = 1$

- $A = DA_{11} + D'A_{12} = \begin{bmatrix} -DR_g & -1 \\ 1 & -1/R \end{bmatrix}$
- $B = DB_{11} + D'B_{12} = \begin{bmatrix} D \\ 0 \end{bmatrix}$
- $(A_{11} - A_{12}) = \begin{bmatrix} -R_g & 0 \\ 0 & 0 \end{bmatrix}$
- $(B_{11} - B_{12}) = \begin{bmatrix} 1 & 0 \\ 0 & 0 \end{bmatrix}$
- $\circ C_1 - C_2 = [1 \ 0]$

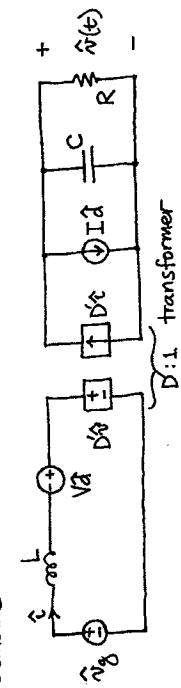
Problem 7.2



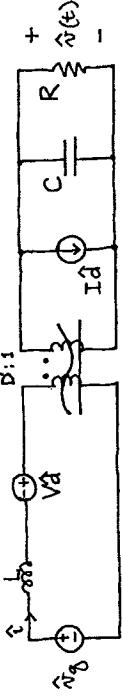
$$C \frac{d\hat{V}_g(t)}{dt} = D' \hat{I}_L(t) - I_d(t) - \frac{\hat{V}_d(t)}{R}$$



Combine circuits:



- b) Equivalent circuit model



Averaged small-signal AC equivalent circuit model of the ideal CCM boost converter.

$$\circ L \frac{d\hat{I}_L}{dt} = \hat{V}_L(t) = -DR_g \hat{I}_L - \hat{V}_C + D\hat{V}_g - R_g \hat{I}_L \hat{I}_d + V_g \hat{I}_d$$

$$\circ C \frac{d\hat{V}_C}{dt} = \hat{I}_C = \frac{\hat{V}_C}{L - R}$$

$$\circ \hat{I}_g = \hat{D}\hat{I}_L + \hat{I}_d$$

