#### **HBT** basics

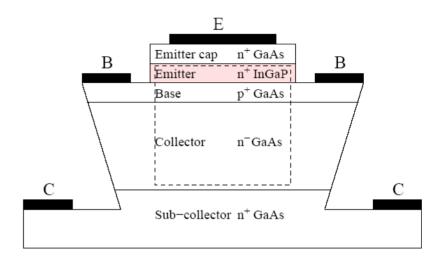
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#### LECTURE 15

- Applications
- Structure
- Energy band diagram
- Collector current

#### HBTs enable portable wireless products





Why does this PDA need HBTs?

#### A DIFFERENTIAL HBT POWER CELL AND ITS MODEL

#### Dong Ho Lee,<sup>1</sup> Yue Chen,<sup>2</sup> Kyung-Ai Lee,<sup>3</sup> and Songcheol Hong<sup>3</sup>

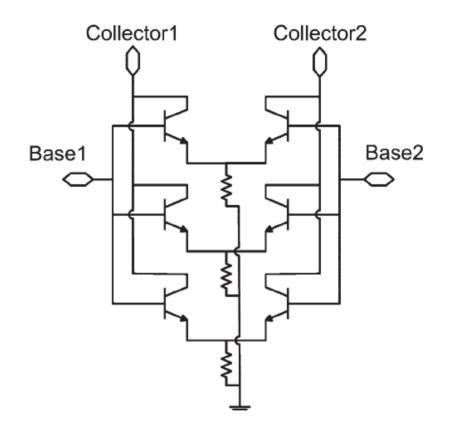
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**ABSTRACT:** A differential heterojunction bipolar transistor (HBT) power cell has been designed and modeled with additional model extraction patterns. The differential power cell, which is composed of a unit differential amplifier with a common emitter ballast resistor, has no gain degradation by the ballast resistors and has been implemented in InGaP/GaAs HBT technology. DC and AC characteristics are extracted from a half circuit of the differential power cell and thermal characteristics are extracted from a common-mode circuit of that. Using the extracted model, a 5-GHz differential power amplifier has been designed and fabricated with on-chip output networks. The 5-GHz differential power amplifier delivers 26 dBm of P<sub>1dB</sub> with 30% collector efficiency. © 2008 Wiley Periodicals, Inc. Microwave Opt Technol Lett 50: 2262–2268, 2008; Published online in Wiley Inter-Science (www.interscience.wiley.com). DOI 10.1002/mop.23684



#### A 1.4-dB-NF Variable-Gain LNA with Continuous Control for 2-GHz-band Mobile Phones Using InGaP Emitter HBTs

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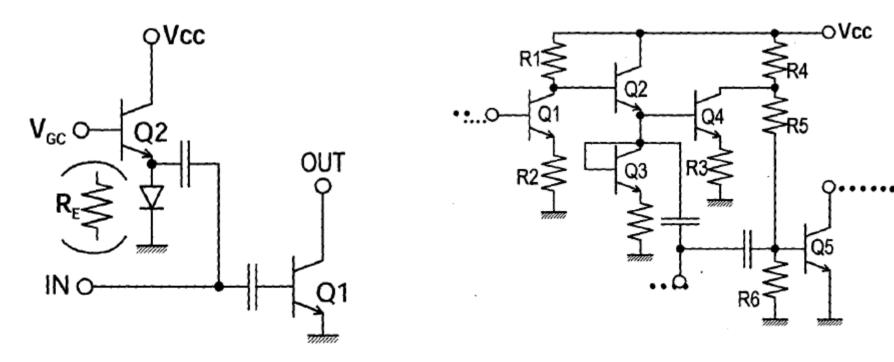
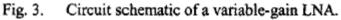
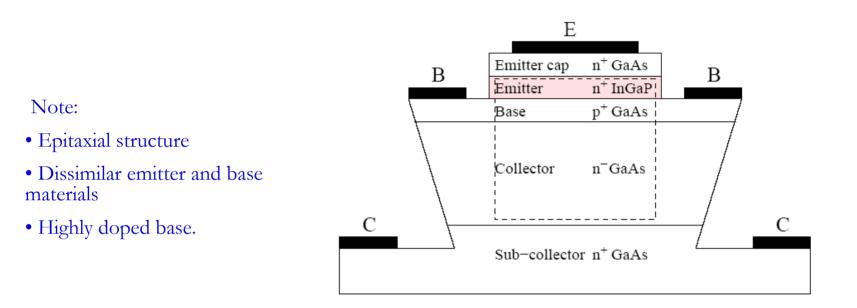


Fig. 1. VG-LNA circuit with input-bypassing by using a diode-loaded emitter follower.

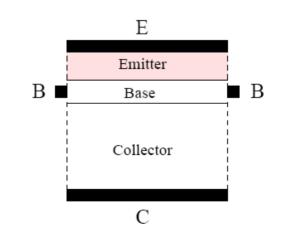


#### IEEE RF IC Symposium, pp. 231-234, 2002

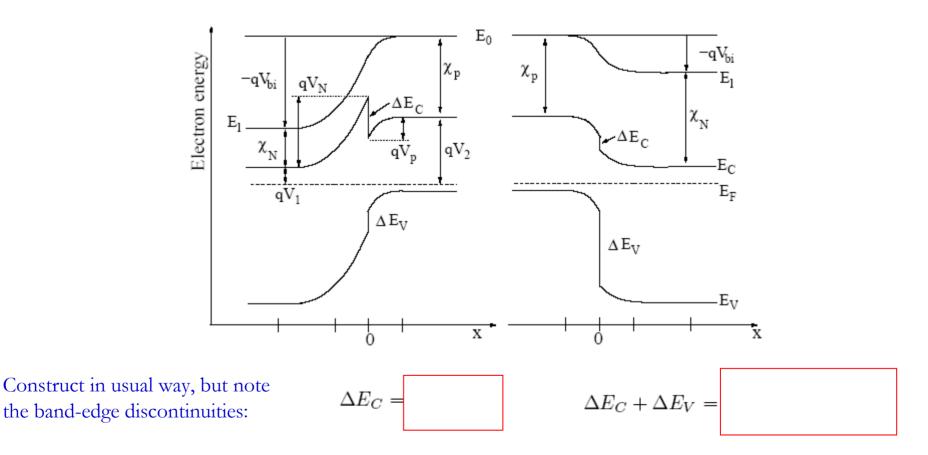
### **HBT** structure



Simplified 1-D structure

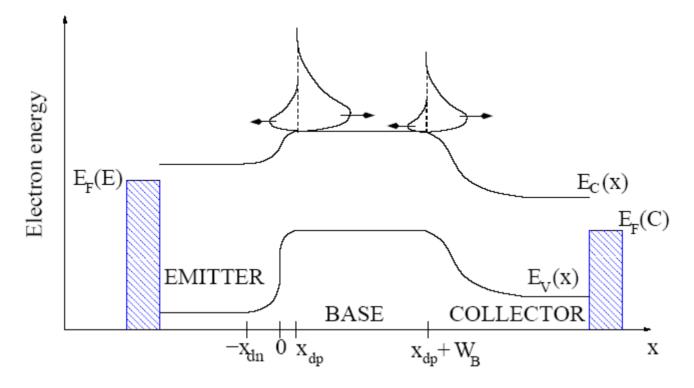


## **Energy band diagrams for HBTs**



What materials are represented in the above band diagrams?

### Preparing to predict I<sub>c</sub>



Go to the toolbox and select the equations needed

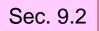
$$\nabla^{2}\psi = \frac{q}{\epsilon}[p - n + N_{D} - N_{A}]$$

$$J_{e} = -qn\mu_{e}\nabla\psi + qD_{e}\nabla n$$

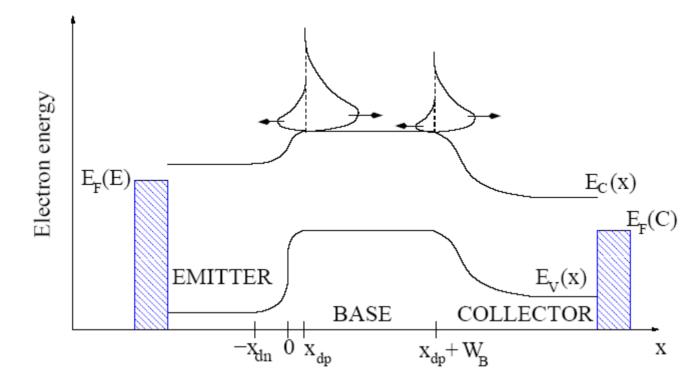
$$J_{h} = -qp\mu_{h}\nabla\psi - qD_{h}\nabla p$$

$$\frac{\partial n}{\partial t} = \frac{1}{q}\nabla \cdot J_{e} - \frac{n - n_{0}}{\tau_{e}} + C_{op}$$

$$\frac{\partial p}{\partial t} = -\frac{1}{q}\nabla \cdot J_{h} - \frac{p - p_{0}}{\tau_{h}} + G_{op}$$



### Setting up for the I<sub>c</sub> derivation



 $W_B$  can be as small as 30nm.

 $N_{\rm B}$  can be as high as 1E19-1E20 cm  $^{-3}$ 

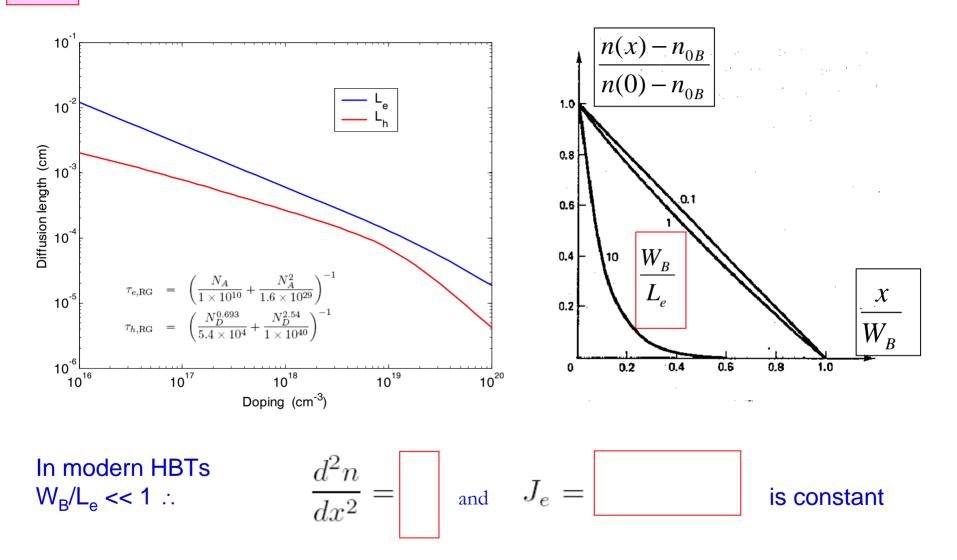
What is  $W_B/L_e$  ?

What is the minority carrier profile in the base?

What is the expression for the electron current in the base?

What are the boundary conditions?

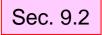
# Answering the questions from the previous slide



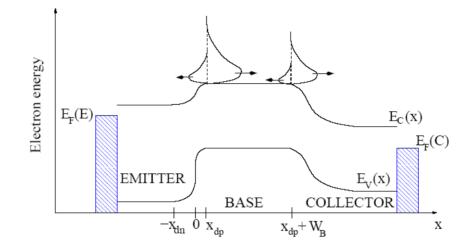
Now we just need the boundary conditions

Sec.

9.2



### BC's for I<sub>C</sub> derivation



New boundary conditions

$$n(x_{dp}) = \frac{n_E^*}{2} + n_L$$
$$J_e(x_{dp}) = -q \frac{n_E^*}{2} 2v_R - (-qn_L 2v_R)$$

What is  $n_E^*$ ?

Why do we need a new BC?

What is the BC at the other end of the QNB?

$$n(x_{dp}) = n_E^* +$$

This is a modified Shockley BC

#### **Collector current: controlling velocities**

Substitute for the carrier concentrations at the boundaries

$$J_e = -qn_{0B} \left[ e^{qV_{BE}/kT} - e^{qV_{BC}/kT} \right] \left[ \frac{W_B}{D_e} + \frac{1}{v_R} \right]^{-1}$$

Note:

Sec. 9.2

- the reciprocal velocities
- estimate typical values
- inclusion of  $v_R$  necessary in modern HBTs

