

- 2 1(a) To combat the effect of decreasing  $C_{ox}$  on  $V_T$ . i.e., to keep  $V_T$  high enough for acceptably low  $I_{subt}$ .
- 2 (b) Halo doping serves to confine the field at the S & D. i.e., to prevent DIBL.
- 2 (c) 50nm FET  $\therefore$  need to use LEVEL 49 from (10.48),  $I_{Dsat}$  is not directly  $\propto$  to  $\mu_{eff}$ .
- This is because the <sup>drift</sup> velocity is limited to  $v_{sat}$ , and not unconstrained to  $\mu_{eff} E_x$ .

$$3 \quad 1(d) \quad S = \frac{\partial V_{GS}}{\partial \log_{10} I_D} = 2.303 m V_{TH} \quad (13.10)$$

$$m = 1 + \frac{\gamma}{2\sqrt{2\phi_B + V_{SB}}} \quad (10.36)$$

$$\gamma = \frac{\sqrt{2q\epsilon_s N_A}}{C_{ox}} \quad \text{following (10.16).}$$

$$C_{ox} = \epsilon_{ox} / t_{ox}.$$

$$m = 1.18 \text{ CMOS90} \quad m = 1.23 \text{ CMOS65}$$

\(\therefore\) CMOS90 needs the smaller \(\Delta V\_{GS}\).

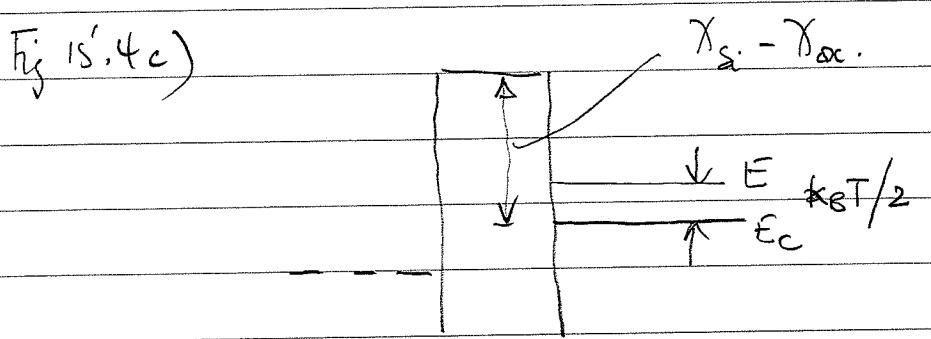
$$3 \quad 1(e) \quad V_T = V_{fb} + 2\phi_B + \gamma\sqrt{2\phi_B + V_{SB}} \quad (10.35).$$

$$V_{fb} = -V_{bi} = \frac{\Phi_g - \Phi_s}{q} \quad \therefore V_{fb} \propto \Phi_g$$

$$\therefore V_{fb}(N_i) > V_{fb}(P_i) \quad \therefore \underline{V_T(N_i) > V_T(P_i)}$$

4 2(a) Fig. 15.4(d)

4 2(b) Approximate by rectangular barrier,



$$T \approx \exp \left[ -\frac{2d}{\hbar} \sqrt{2m^* (U_2 - E)} \right]$$

$$\ln T = -\frac{2d}{\hbar} \sqrt{2m^* (U_2 - E)}$$

$$d = -\ln T \cdot \frac{\hbar}{2 \sqrt{2m^* (U_2 - E)}}$$

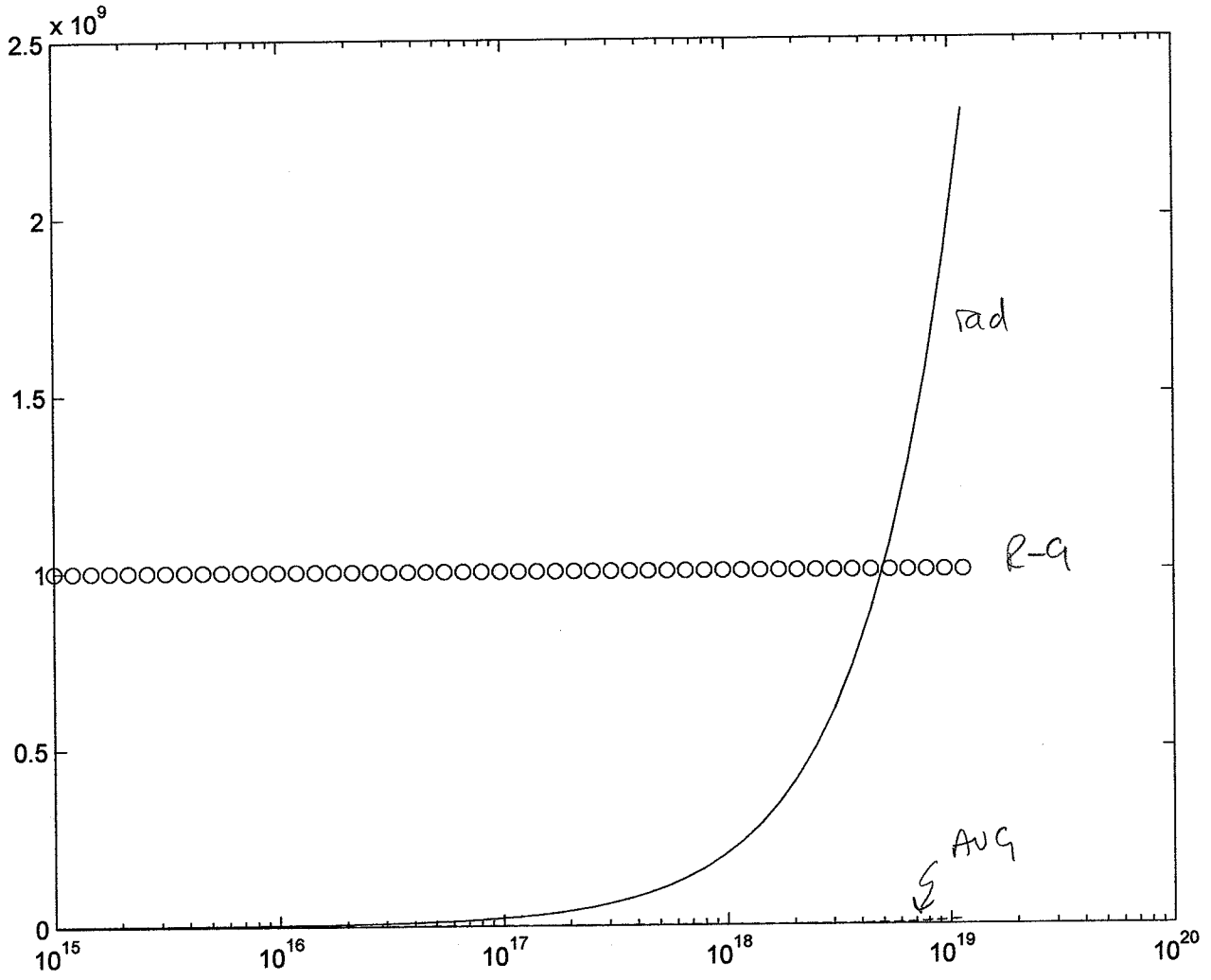
$$m^* (\text{SiO}_2) = 0.3 \times 9.1 \times 10^{-31} \text{ kg} \quad \hbar = 1.05 \times 10^{-34} \text{ Js}$$

$$(U_2 - E) = (\chi_{Si} - \chi_{ox}) - \frac{3}{2} k_B T = (4.01 - 0.9) - \frac{3}{2} \times 0.0259 \text{ eV} = 3.071 \text{ eV} \approx 4.914 \times 10^{-19} \text{ J}$$

$$d = -\ln T \cdot 1.014 \times 10^{-10} \rightarrow 7 \text{ nm for } T = 1 \times 10^{-30}$$

4 2(c) (15.6)  $V_B' = \frac{V_{DD}}{2} \left[ \frac{C_b - C_{st}}{C_{st} + C_b} \right] \rightarrow \frac{V_{DD} - \Delta V}{2}$

$$\frac{C_b - C_{st}}{C_{st} + C_b} = 1 - \frac{2\Delta V}{V_{DD}} = 1 - 0.02 = 0.98 \rightarrow \underline{C_b = 99 \text{ pF}}$$



$S^{-1}$

$S \text{ AUG}$

$\ln \text{ cm}^{-3}$

$$1 \quad 3 \quad (a) \quad WPE = \frac{S_{out}}{\overline{P}_{in}} = \eta_v \cdot \eta_c \cdot \eta_{rad} \cdot \eta_{ext}$$

$$2 \quad \eta_v = \frac{E_g}{qV_a} = \frac{1.42}{1.25} = 1.14$$

$$2 \quad \eta_c = \frac{J_{achiev}}{\overline{J_s}} = 0.9$$

$$\eta_{ext} = 0.5$$

$$\eta_{rad} = \frac{1}{\frac{I_{rad}}{1/2e}}$$

$$3 \quad I_{rad} = \frac{1}{B(p_0 + \Delta n)} \quad \eta_e = \frac{1}{A} \quad I_{Ag} =$$

$$\eta_{rad} = 0.66$$

$$\therefore WPE = 1.14 \times 0.9 \times 0.5 \times 0.66 = \underline{\underline{33.9\%}}$$

$$4 \quad (b) \quad \text{Luminous } \eta = \frac{\Phi}{I_D V_D} \quad \Phi = 683 \gamma S_{out}$$

$$\approx 0$$

3(b) cont. For monochromatic light  $\lambda = 683 \text{ \AA}$  Sent

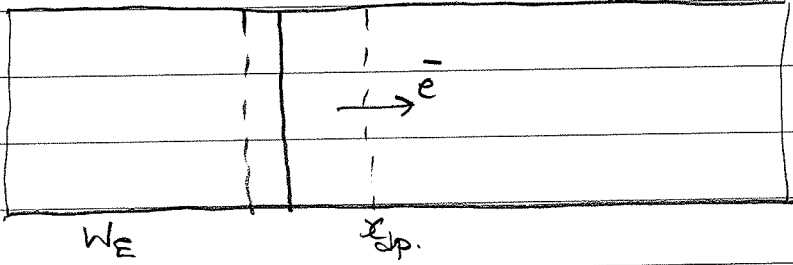
For GaAs,  $E_g = 1.42 \text{ eV} = \frac{hc}{\lambda}$

$\lambda = \frac{6.63 \times 10^{-34} \times 3 \times 10^8}{1.42 \times 1.6 \times 10^{-19}} = \frac{1.24 \times 10^{-6}}{1.42} = 875 \text{ nm}$

From Fig. 8.7,  $\delta \approx 0$

$\therefore$  Luminous  $\eta \approx 0$

4a)



4  
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$I_0 = I_{oh} + I_{oe}$

$I_{oe} = -q A n_{op} \frac{D_e}{L_e}$

Ideal diode (6.37).

$I_{oh} = -q A p_{on} \frac{D_h}{L_h} \text{ or } \frac{W_E}{L_h}$

(Assignment 2, Q4)

$\rightarrow -q A p_{on} \frac{D_h}{L_h} \cdot \frac{L_h}{W_E}$

$W_E \ll L_e$  (Mid-term)

$= -q A p_{on} \frac{D_h}{W_E}$

$\therefore I_0 = -q A \left[ n_{op} \frac{D_e}{L_e} + p_{on} \frac{D_h}{W_E} \right]$

(6)

4b)

$$N_D = 10^{19} \text{ cm}^{-3}, \quad N_A = 10^{16} \text{ cm}^{-3}$$

$$\mu_h = 65 \text{ cm}^2 \text{ V}^{-1} \text{ s}^{-1}, \quad \tau_h = \frac{5 \times 10^{-7}}{1 + 200} = 2.5 \times 10^{-9} \text{ s.}$$

$$D_h = \frac{kT}{q} \mu_h = 1.68 \text{ cm}^2 \text{ s}^{-1}$$

$$L_h = \sqrt{D_h \tau_h} = 6.48 \times 10^{-5} \text{ cm} = 648 \text{ nm}$$

$$W_E = 100 \text{ nm}$$

$$\mu_e = 1258 \text{ cm}^2 \text{ V}^{-1} \text{ s}^{-1}, \quad D_e = 32.6 \text{ cm}^2 \text{ s}^{-1}, \quad \tau_e = \frac{5 \times 10^{-7}}{1 + 2 \times 10^{16} \times 10^{-17}} = 4.17 \times 10^{-7} \text{ s.}$$

$$L_e = 3.69 \times 10^{-3} \text{ cm.}$$

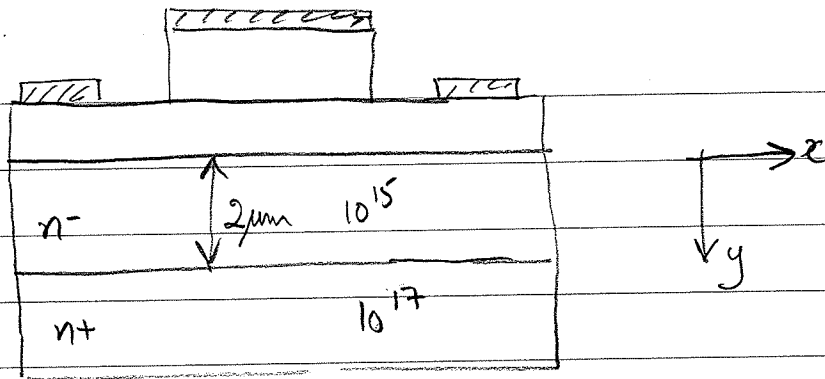
$$p_{in} = \frac{(9.5 \times 10^9)^2}{10^{19}} = 9.025 \text{ cm}^{-3}, \quad n_{pp} = 9.025 \times 10^3$$

$$\begin{aligned} \therefore I_0 &= -q A \left[ \frac{9.025 \times 10^3 \times 32.6}{3.69 \times 10^{-3}} + \frac{9.025 \times 1.68}{100 \times 10^{-7}} \right] \\ &= -1.6 \times 10^{-17} \left[ 7.97 \times 10^7 + 1.516 \times 10^6 \right] \\ &= 1.3 \times 10^{-9} \text{ A} \end{aligned}$$

$$2 \quad c) \quad V_{oc} = V_T \ln \left( \frac{I_{ph} + I_0}{I_0} \right) \approx V_T \ln \frac{I_{ph}}{I_0} = \underline{0.57 \text{ V.}}$$

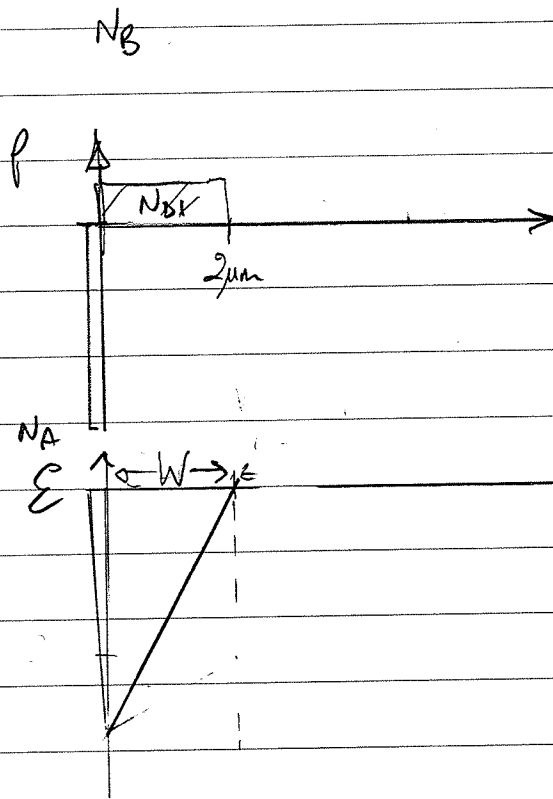
$$2 \quad d) \quad \frac{I_{ph} V_{oc}}{S \cdot A} = \eta, \quad FF = \frac{100 \times 10^{-3} \times 100 \times 0.2}{4 \times 0.57} = \underline{0.877}$$

5(a)



2,2 (i) High  $BDV$ , low  $R_c$

(ii)



$$W = \sqrt{\frac{2\epsilon_s}{q} (V_{bi} - V_a) \left( \frac{1}{N_B} + \frac{1}{N_C} \right)}$$

Assume all of  $W$  is in the collector

Assume  $|-V_a| \gg V_{bi}$

$$\therefore -V_a = V_{bc} = \frac{W^2 q}{2\epsilon_s} \frac{1}{N_C}$$



b(i) cont

$$V_{bc} = \frac{4 \times 10^{-12} \times 10^{22} \times 1.6 \times 10^{-19}}{2 \times 12.9 \times 8.85 \times 10^{-12}} = 28 \text{ V}$$

$$b(ii) \quad E = -d\phi/dx \quad \rightarrow \quad -d\phi = \int E dx$$

$$28 = \frac{1}{2} E_{max} \cdot W$$

$$E_{max} = \frac{56}{2 \times 10^{-6}} = 28 \text{ V}/\mu\text{m}$$

$$= 28 \times 10^{-6} \text{ MV}/\mu\text{m}$$

$$= 28 \times 10^{-6} \times 10^4 \text{ MV/cm}$$

$$= \underline{0.28 \text{ MV/cm}}$$

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Neatly breaks down!

$$c) \quad f_T = \frac{g_m}{C_{\pi} + C_{\mu} (1 + g_m (R_e + R_c))} \quad (14.16)$$

$$g_m = \frac{I_e}{V_T}, \quad I_e \propto A$$

$$C_{\pi} \propto A, \quad C_{\mu} \propto A, \quad R_e \propto \frac{1}{A}$$

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$$R_c \propto \frac{\rho l}{a} \quad \text{[Diagram of a rectangular block with length } l, \text{ width } l, \text{ and height } a \text{]} \quad = \rho \frac{l}{ld} \quad \text{i.e. doesn't scale}$$

$$\therefore \text{New } f_T = \frac{g_m A}{C_{\pi} A + C_{\mu} A (1 + g_m A (\frac{R_e}{A} + R_c))}$$

A=1/4 ∴ new fT higher.

$$= \frac{g_m}{C_{\pi} + C_{\mu} (1 + g_m (R_e + R_c A))}$$