

$$1 (a) \quad \Phi = \Phi_0 e^{-\alpha x}$$

$$\frac{\partial P}{\partial t} + \nabla \cdot \Phi = R_{\text{rad}} - A \quad (7.8)$$

Steady-state, no  $R_{\text{rad}}$ ,  $A = G_{\text{op}}$ , 1-D

$$\frac{d\Phi}{dx} = -G_{\text{op}}$$

$$\underline{-\alpha \Phi_0 e^{-\alpha x} = -G_{\text{op}}}$$

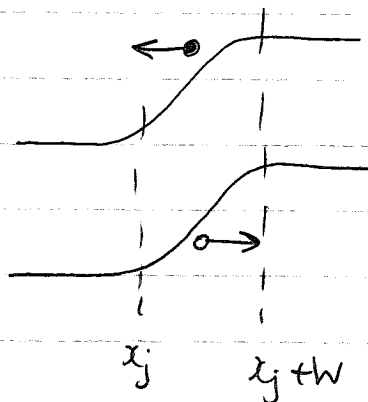
This is (7.11)

(b) From equation tool set:

$$-\frac{1}{q} \frac{dJ_e}{dx} = G_{\text{op}} - U \quad (5.24)$$

$U \approx 0$  in depletion region

$$\int_{J_e(x_j)}^{J_e(x_j+w)} dJ_e = -q \int_{x_j}^{x_j+w} G_{\text{op}} dx$$



$$\begin{aligned} J_e \Big|_{J_e(x_j)}^0 &= -q \int_{x_j}^{x_j+w} \alpha \Phi_0 e^{-\alpha x} dx \\ -J_e(x_j) &= q \Phi_0 e^{-\alpha x} \Big|_{x_j}^{x_j+w} = q \Phi_0 \left( e^{-(x_j+w)\alpha} - e^{-\alpha x_j} \right) \\ &= q \Phi_0 e^{-\alpha x_j} \left[ e^{-\alpha w} - 1 \right] \end{aligned}$$

$$\underline{J_e(x_j) = q \Phi_0 e^{-\alpha x_j} \left[ 1 - e^{-\alpha w} \right]} \quad (7.18)$$

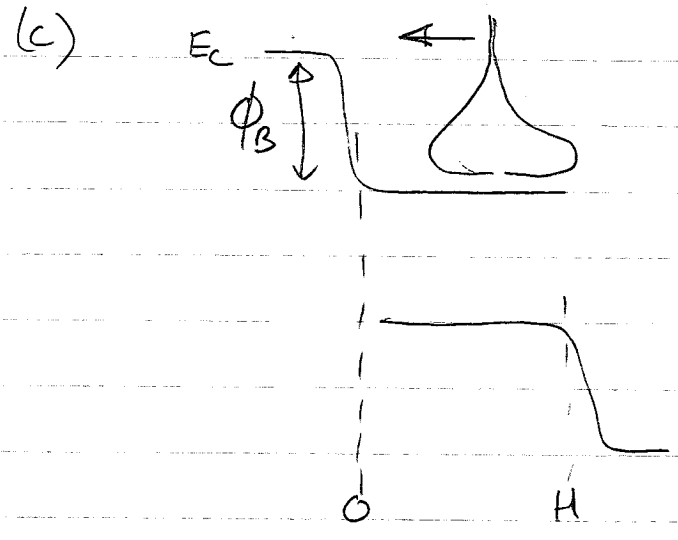
$$(c) \quad x_j = 0; \quad J_e = 1.6 \times 10^{-19} \times 6.25 \times 10^{20} \left[ 1 - e^{-10^5 \cdot 10^{-4}} \right] = \underline{100 \text{ A/m}^2}$$

2 (a) From Fig 8.7 (Fig. 1 of exam), luminous efficacy of 68.3 lm/w i.e.  $\gamma = 0.1$ , occurs in the blue @  $\approx 470\text{nm}$ .

$$E = hc/\lambda = \left[ \frac{6.63 \times 10^{-34} \times 3 \times 10^8}{470 \times 10^{-9}} \right] / 1.6 \times 10^{-19} \text{ in eV}$$

$$E \equiv E_g = \underline{\underline{2.645 \text{ eV}}}$$

(b)  $\eta_v = \frac{E_g}{qV_a} = \frac{2.645}{2.64} = \underline{\underline{1.002}} \quad (8.1)$



No hole escape @ H  
 $\therefore J_e(H) = J_{\text{Diode}}$   
 $I_e(H) = 10 \times 10^{-3} \text{ A}$

Electron escape current at 0 due to thermionic emission

$$J_e(x=0) = -q \frac{n}{2} 2v_r (-\bar{x}) e^{-\phi_B/k_B T}$$

$$I_e(0) = 1.6 \times 10^{-19} \times 10^{19} \times 10^5 e^{-0.3/0.0259} \times (5 \times 10^{-8})^2$$

$$= 37.3 \mu\text{A}$$

$$\therefore \eta_c = \frac{10 \times 10^{-3} - 37.3 \times 10^{-6}}{10 \times 10^{-3}} = \frac{10 - 0.0373}{10} = \underline{\underline{0.996}}$$

$$= \frac{J_e(H) - J_e(0)}{J_D} \quad (8.5)$$

2(d)  $\Delta n > p_0 \therefore$  high-level injection

$$\begin{aligned} \tau_{e,rad} &= \frac{1}{B(p_0 + \Delta n)} & (3.19) \\ &= \frac{1}{2 \times 10^{-10} \times (10^{16} + 10^{19})} = \frac{5 \times 10^{-10} \text{ s}}{} \end{aligned}$$

$$\begin{aligned} (e) \quad \tau_e &= \left[ \frac{1}{\tau_{non-rad}} + \frac{1}{\tau_{rad}} \right]^{-1} & (3.24) \\ &= \left[ \frac{1}{10^{-9}} + \frac{1}{5 \times 10^{-10}} \right]^{-1} = 3.33 \times 10^{-10} \text{ s} \end{aligned}$$

$$\eta_{rad} = \frac{\tau_e}{\tau_{rad}} \quad (8.7) = \frac{3.33 \times 10^{-10}}{5 \times 10^{-10}} = \underline{\underline{0.667}}$$

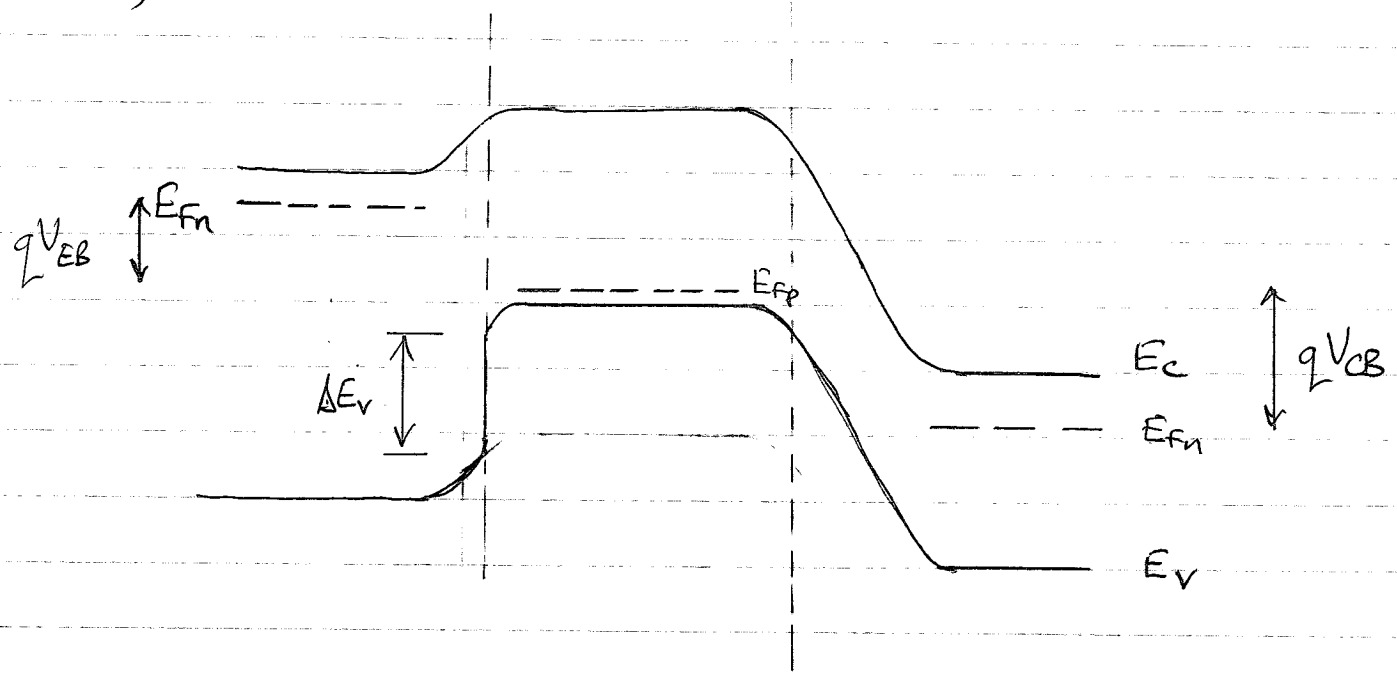
(f) luminous efficiency = wall-plug efficiency  $\times$  lum. efficacy (8.16)

$$40 = \text{WPE} \times 68.3 \quad \Rightarrow \quad \text{WPE} = 0.586$$

$$\text{WPE} = \eta_v \eta_c \eta_{rad} \eta_{ext} \quad (8.12)$$

$$\begin{aligned} \therefore \eta_{ext} &= \frac{0.586}{(1.002 \times 0.996 \times 0.667)} \\ &= \underline{\underline{0.88}} \end{aligned}$$

3(a)



(b)  $\Delta E_g = \Delta E_c + \Delta E_v$ ,  $\Delta E_c = \Delta \chi = 0$  \*  $\therefore$  No extra barrier for  $J_E$   
 $\therefore \Delta E_v = \Delta E_g = 1.85 - 1.42 = 0.47 \text{ eV}$

\* This large barrier suppresses the hole back-injection current.  
 $\therefore J_B$  is reduced

$\therefore$  with  $J_E$  unaffected &  $J_B$  reduced,  $\beta$  can be high

(c)  $f_{max} = \sqrt{\frac{f_{Ti}}{8\pi R_b C_{bc}}}$  (14.33),  $f_{Ti} = \frac{g_m}{2\pi(C_{be} + C_{bc})}$  (14.16)

$g_m = \left| \frac{\partial I_c}{\partial V_{BE}} \right| = \frac{q}{V_{TE}} n_{os} e \cdot \frac{1}{\frac{w_B}{D_e} + \frac{1}{v_e}}$

High doping in the base is the important feature, and is made possible by  $\Delta E_v$ . However, it lowers  $n_{os}$ , which counteracts

3c, cont) The reduction in  $W_B$ , so there's not much advantage re: gm.

$C_{EB,j}$  may be slightly affected because of  $\epsilon_N \neq \epsilon_p$  (6.42)

$C_{EB,b}$  reduced because of altered narrow base.

The big factor is  $R_b$ . This is a lateral R (Fig. 14.5), and is reduced directly by  $N_B$  (14.37).

4 (a) Fig. 10.14 shows that LEVEL 1 overestimates  $I_{sat}$  for  $L = 100\text{nm}$ , so will definitely overestimate for  $L = 65\text{nm}$ .  
Level 1 assumes  $\mu = \mu_0$ , i.e.  $v = \mu_0 E_x$

So, as  $E_x \uparrow$  with  $L \downarrow$   $v$  becomes unreasonably high. In LEVEL 4,  $v$  is restricted to  $v_{max} = v_{sat}$ , thereby reducing the saturation current.

(b) In triode mode, 
$$I_D = Z C_{ox} \left[ V_{GS} - V_T - m \frac{V_{DS}}{2} \right] \cdot \mu_{eff} \frac{V_{DS}}{L + \mu V_{DS}/v_{sat}} \quad (10.47)$$

$$\equiv k \left[ V_{GS} - V_T - m \frac{V_{DS}}{2} \right] \quad k = \text{constant}$$

when  $I_D = 0$ , 
$$V_{GS} = V_T + m \frac{V_{DS}}{2} = 0.44\text{V}$$

$$m = 1 + \frac{\gamma}{2\sqrt{2}\phi_B} \quad (10.36), \quad \gamma = \frac{1}{C_{ox}} \sqrt{2q\epsilon_s N_A} \quad (10.16) \quad \phi_B = V_{th} \ln \frac{N_A}{n_i} \quad (10.5)$$

$$\rightarrow \gamma = V^{1/2}, \quad 2\phi_B = V, \quad m = 1.23$$

$$\therefore V_T = 0.44 - \frac{1.23 \times 0.2}{2} = \underline{\underline{0.317\text{V}}}$$

$$4(c) \quad \text{Long-channel } V_T = V_{fb} + 2\phi_B + \gamma \sqrt{2\phi_B}$$

$$V_{fb} = \bar{\Phi}_g - \bar{\Phi}_s \equiv -E_g/2 - \phi_B = -1.07 \text{ V}$$

$$2\phi_B = 1.00 \text{ V}$$

$$\gamma \sqrt{2\phi_B} = 0.46 \text{ V}$$

$$\therefore \underline{\underline{V_T (\text{long channel}) = 0.40 \text{ V}}}$$

This is less than the measured value because it does not account for the  $V_T$  reduction that occurs in practice in short FETs due to the short-channel effect.

(d) To keep  $V_T$  at a high-enough value so as not to produce excessively high  $I_{\text{sub-threshold}}$ . This counters the effect of  $t_{\text{ox}}$ : its scaling down increases  $C_{\text{ox}}$  and reduces  $V_T$ .

Future FETs will be very small, so the actual number of dopant atoms will be small.

e.g. 5 atoms in  $5 \times 10 \times 10 \text{ nm}^3$  FET with  $N_A = 10^{19} \text{ cm}^{-3}$ .

5(a) Read current.  $I_{Dsat} = \frac{Z}{L} \mu C_{ox} \left( \frac{V_{GS} - V_T}{2m} \right)^2$  (10.38)

$$\equiv \frac{Z}{L} K \left( \frac{V_{GS} - V_T}{2m} \right)^2$$

$$10^{-3} = 1 \cdot K \cdot \left( \frac{1.25 - 0.25}{2 \times 1} \right)^2$$

$$\therefore \underline{\underline{K = 2 \times 10^{-3} \text{ A/V}^2}}$$

(b)  $n = \log_2 \left( \frac{I_{max}}{\Delta I} + 1 \right)$  (15.3)

$$\therefore 2^2 = \frac{10^{-3}}{\Delta I} + 1 \quad \rightarrow \quad \underline{\underline{\Delta I = \frac{10^{-3}}{3} \text{ A}}}$$

(c) From (10.38) using K as above

$$\frac{dI_{Dsat}}{dV_T} = \frac{Z}{L} \cdot \frac{K}{2m} \cdot 2(V_{GS} - V_T) (-1) = -\frac{Z}{L} \frac{K}{m} (V_{GS} - V_T)$$

$$\therefore \Delta V_T = -\Delta I \cdot \frac{Lm}{ZK(V_{GS} - V_T)} = \underline{\underline{\frac{-\Delta I}{K(V_{GS} - V_T)}}}$$

(d)  $\Delta V_T = -\frac{\Delta Q_F}{C_{ox, top}}$  (15.2) ;  $C_{ox, top} = \frac{\epsilon_{ox}}{L_{ox}} = \frac{3.9 \times 8.85 \times 10^{-12}}{18 \times 10^{-9}}$   
 $= 1.918 \times 10^{-3} \text{ F/m}^2$

$$\Delta N_F = -\frac{\Delta Q_F A}{-q} = \frac{\Delta V_T \cdot C_{ox} \cdot A}{-q} = \frac{\Delta I C_{ox} \cdot A}{qK(V_{GS} - V_T)}$$

$$= \frac{10^{-3} \times 1.918 \times 10^{-3} \times (100\sqrt{10} \times 10^{-9})^2}{3 \times 1.6 \times 10^{-19} \times 2 \times 10^{-3} \times 1} = \underline{\underline{200}} \text{ electrons}$$

More on 5(c)

$$I_{\text{Dsat}} = \frac{K}{2m} (V_{\text{GS}} - V_{\text{T}})^2 = \text{with case } \frac{K}{2} (V_{\text{GS}} - V_{\text{T}})^2$$

Calculus gives  $\Delta I_{\text{Dsat}} = -\Delta V_{\text{T}} \cdot K (V_{\text{GS}} - V_{\text{T}})$

Non-Calculus;  $\Delta I = \frac{K}{2} \left[ (V_{\text{GS}} - V_{\text{T1}})^2 - (V_{\text{GS}} - V_{\text{T0}})^2 \right]$

$$= \frac{K}{2} \left[ \cancel{V_{\text{GS}}^2} - 2V_{\text{GS}}V_{\text{T1}} + V_{\text{T1}}^2 - \cancel{V_{\text{GS}}^2} + 2V_{\text{GS}}V_{\text{T0}} - V_{\text{T0}}^2 \right]$$
$$= \frac{K}{2} \left[ 2V_{\text{GS}}(V_{\text{T0}} - V_{\text{T1}}) + V_{\text{T1}}^2 - V_{\text{T0}}^2 \right]$$

Let  $V_{\text{T1}} - V_{\text{T0}} = \Delta V_{\text{T}}$

$$\equiv \frac{K}{2} \left[ -2V_{\text{GS}} \Delta V_{\text{T}} + \cancel{V_{\text{T1}}^2} + \cancel{V_{\text{T0}}^2} + 2\Delta V_{\text{T}}V_{\text{T0}} - \cancel{V_{\text{T0}}^2} \right]$$
$$= \frac{K}{2} \left[ 2\Delta V_{\text{T}} (+V_{\text{GS}} + V_{\text{T0}}) + \Delta V_{\text{T}}^2 \right]$$
$$= -\Delta V_{\text{T}} (V_{\text{GS}} - V_{\text{T}}) \cdot K + \frac{K \Delta V_{\text{T}}^2}{2}$$

Calculus refers to  $\lim_{\Delta x \rightarrow 0}$ , i.e. neglect the  $\Delta V_{\text{T}}^2$  term.

If it is included:  $\frac{\Delta I}{K} = -\Delta V_{\text{T}} (V_{\text{GS}} - V_{\text{T}}) + \frac{\Delta V_{\text{T}}^2}{2}$

$$\Delta V_{\text{T}}^2 - \Delta V_{\text{T}} (2(V_{\text{GS}} - V_{\text{T}})) - \frac{2\Delta I}{K} = 0$$

$$\Delta V_{\text{T}}^2 - 2\Delta V_{\text{T}} - \frac{1}{3} = 0$$

$$\Delta V_{\text{T}} = \frac{2 \pm \sqrt{4 + \frac{4}{3}}}{2} = \frac{2 \pm \sqrt{\frac{16}{3}}}{2} = 2 - \frac{4}{1.732} = \underline{\underline{-0.1547V}}$$

Compare with Calculus:  $\Delta V_{\text{T}} = \underline{\underline{-0.1667V}}$